

United
States
of
America



To Promote the Progress



of Science and Useful Arts

The Director

of the United States Patent and Trademark Office has received an application for a patent for a new and useful invention. The title and description of the invention are enclosed. The requirements of law have been complied with, and it has been determined that a patent on the invention shall be granted under the law.

Therefore, this United States

Patent

grants to the person(s) having title to this patent the right to exclude others from making, using, offering for sale, or selling the invention throughout the United States of America or importing the invention into the United States of America, and if the invention is a process, of the right to exclude others from using, offering for sale or selling throughout the United States of America, products made by that process, for the term set forth in 35 U.S.C. 154(a)(2) or (c)(1), subject to the payment of maintenance fees as provided by 35 U.S.C. 41(b). See the Maintenance Fee Notice on the inside of the cover.



Katherine Kelly Vidal



DIRECTOR OF THE UNITED STATES PATENT AND TRADEMARK OFFICE

Maintenance Fee Notice

If the application for this patent was filed on or after December 12, 1980, maintenance fees are due three years and six months, seven years and six months, and eleven years and six months after the date of this grant, or within a grace period of six months thereafter upon payment of a surcharge as provided by law. The amount, number and timing of the maintenance fees required may be changed by law or regulation. Unless payment of the applicable maintenance fee is received in the United States Patent and Trademark Office on or before the date the fee is due or within a grace period of six months thereafter, the patent will expire as of the end of such grace period.

Patent Term Notice

If the application for this patent was filed on or after June 8, 1995, the term of this patent begins on the date on which this patent issues and ends twenty years from the filing date of the application or, if the application contains a specific reference to an earlier filed application or applications under 35 U.S.C. 120, 121, 365(c), or 386(c), twenty years from the filing date of the earliest such application (“the twenty-year term”), subject to the payment of maintenance fees as provided by 35 U.S.C. 41(b), and any extension as provided by 35 U.S.C. 154(b) or 156 or any disclaimer under 35 U.S.C. 253.

If this application was filed prior to June 8, 1995, the term of this patent begins on the date on which this patent issues and ends on the later of seventeen years from the date of the grant of this patent or the twenty-year term set forth above for patents resulting from applications filed on or after June 8, 1995, subject to the payment of maintenance fees as provided by 35 U.S.C. 41(b) and any extension as provided by 35 U.S.C. 156 or any disclaimer under 35 U.S.C. 253.



US012148541B2

(12) **United States Patent**
Singh et al.

(10) **Patent No.:** **US 12,148,541 B2**

(45) **Date of Patent:** ***Nov. 19, 2024**

(54) **VENTILATED CASK FOR NUCLEAR WASTE STORAGE**

(71) Applicant: **HOLTEC INTERNATIONAL**,
Camden, NJ (US)

(72) Inventors: **Krishna P. Singh**, Jupiter, FL (US);
Stephen J. Agace, Voorhees, NJ (US);
Robert Mahorter, Ocean City, NJ (US)

(73) Assignee: **HOLTEC INTERNATIONAL**

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

This patent is subject to a terminal disclaimer.

(21) Appl. No.: **18/232,380**

(22) Filed: **Aug. 10, 2023**

(65) **Prior Publication Data**

US 2023/0386692 A1 Nov. 30, 2023

Related U.S. Application Data

(63) Continuation of application No. 17/470,053, filed on Sep. 9, 2021, now Pat. No. 11,735,327.

(60) Provisional application No. 63/223,578, filed on Jul. 20, 2021, provisional application No. 63/211,234, filed on Jun. 16, 2021.

(51) **Int. Cl.**

G21F 5/10 (2006.01)

G21F 5/00 (2006.01)

G21F 5/008 (2006.01)

(52) **U.S. Cl.**

CPC **G21F 5/10** (2013.01); **G21F 5/008** (2013.01)

(58) **Field of Classification Search**

CPC G21F 5/008; G21F 5/10

USPC 250/505.1, 506.1, 507.1, 515.1, 516.1, 250/517.1, 518.1, 519.1

See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

| | | |
|---------------|---------|---------------|
| 4,498,011 A | 2/1985 | Dyck et al. |
| 4,527,066 A | 7/1985 | Dyck et al. |
| 5,839,874 A | 11/1998 | Johnston |
| 6,519,307 B1 | 2/2003 | Singh |
| 6,718,000 B2 | 4/2004 | Singh |
| 6,805,815 B1 | 10/2004 | Soundararajan |
| 8,798,224 B2 | 8/2014 | Singh |
| 8,995,604 B2 | 3/2015 | Singh et al. |
| 9,208,914 B2 | 12/2015 | Singh et al. |
| 10,049,777 B2 | 8/2018 | Singh |

(Continued)

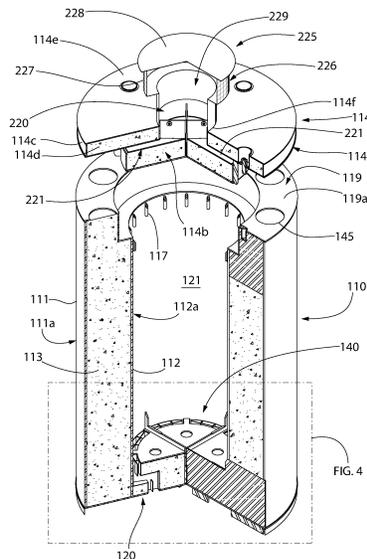
Primary Examiner — Nicole M Ippolito

(74) *Attorney, Agent, or Firm* — The Belles Group, P.C.

(57) **ABSTRACT**

A natural passively cooled ventilated cask includes a cavity which holds a canister containing heat and radiation emitting spent nuclear fuel assemblies or other high level wastes. Ambient ventilation or cooling air is drawn inwards beneath the cask and vertically upwards into a lower portion of the cavity through air inlet ducts formed integrally with a bottom canister support structure coupled to the cask. The air heated by the canister flows upwards in the cavity and returns to atmosphere through air outlet ducts in the cask lid. Air circulation is driven via natural convective thermosiphon flow. Structural standoff members elevate the bottom of the cask above a concrete base pad forming an air inlet plenum beneath the canister support structure. The lateral sidewall surface of the cask has no penetrations for the air inlets, which eliminates any streaming path for radiation emanating from the spent nuclear fuel.

9 Claims, 22 Drawing Sheets



(56)

References Cited

U.S. PATENT DOCUMENTS

| | | | | |
|--------------|-----|---------|--------------|------------------------|
| 10,145,754 | B2 | 12/2018 | Takeda | |
| 10,332,642 | B2 | 6/2019 | Singh | |
| 10,515,730 | B2 | 12/2019 | Singh et al. | |
| 10,714,223 | B2 | 7/2020 | Singh | |
| 10,861,612 | B2 | 12/2020 | Singh et al. | |
| 10,878,973 | B2 | 12/2020 | Singh | |
| 11,043,312 | B2 | 6/2021 | Singh | |
| 11,250,963 | B2 | 2/2022 | Singh | |
| 11,735,327 | B2* | 8/2023 | Singh | G21F 5/10 250/506.1 |
| 2003/0147486 | A1 | 8/2003 | Singh et al. | |
| 2010/0284506 | A1 | 11/2010 | Singh | |
| 2014/0329455 | A1 | 11/2014 | Singh | |
| 2014/0341330 | A1 | 11/2014 | Singh | |
| 2015/0243391 | A1 | 8/2015 | Singh | |
| 2019/0131024 | A1 | 5/2019 | Pfeifer | |
| 2019/0139661 | A1 | 5/2019 | Singh | |
| 2019/0326028 | A1 | 10/2019 | Singh | |
| 2020/0027612 | A1 | 1/2020 | Singh | |
| 2020/0035371 | A1 | 1/2020 | Arai et al. | |
| 2021/0012915 | A1 | 1/2021 | Singh | |
| 2021/0057120 | A1 | 2/2021 | Singh | |
| 2021/0407697 | A1 | 12/2021 | Singh et al. | |

* cited by examiner

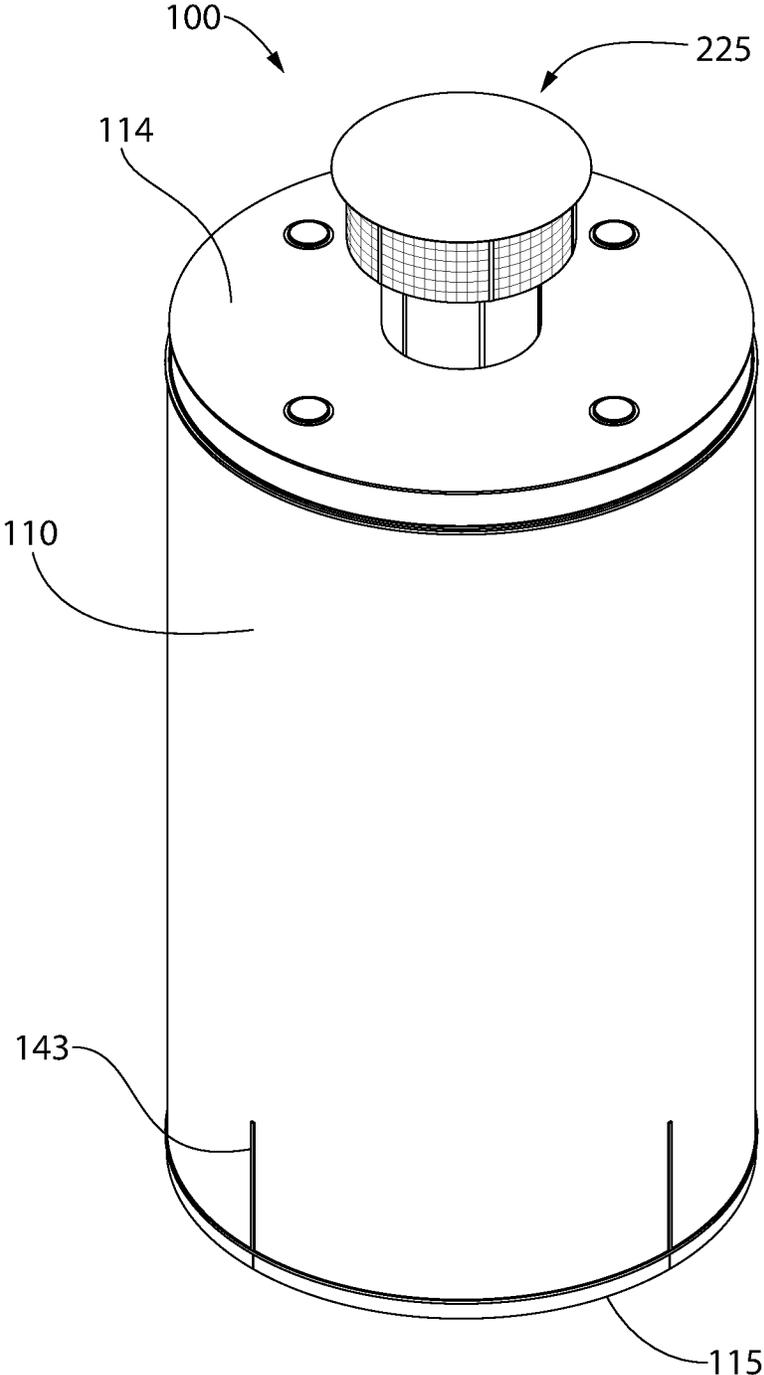


FIG. 1

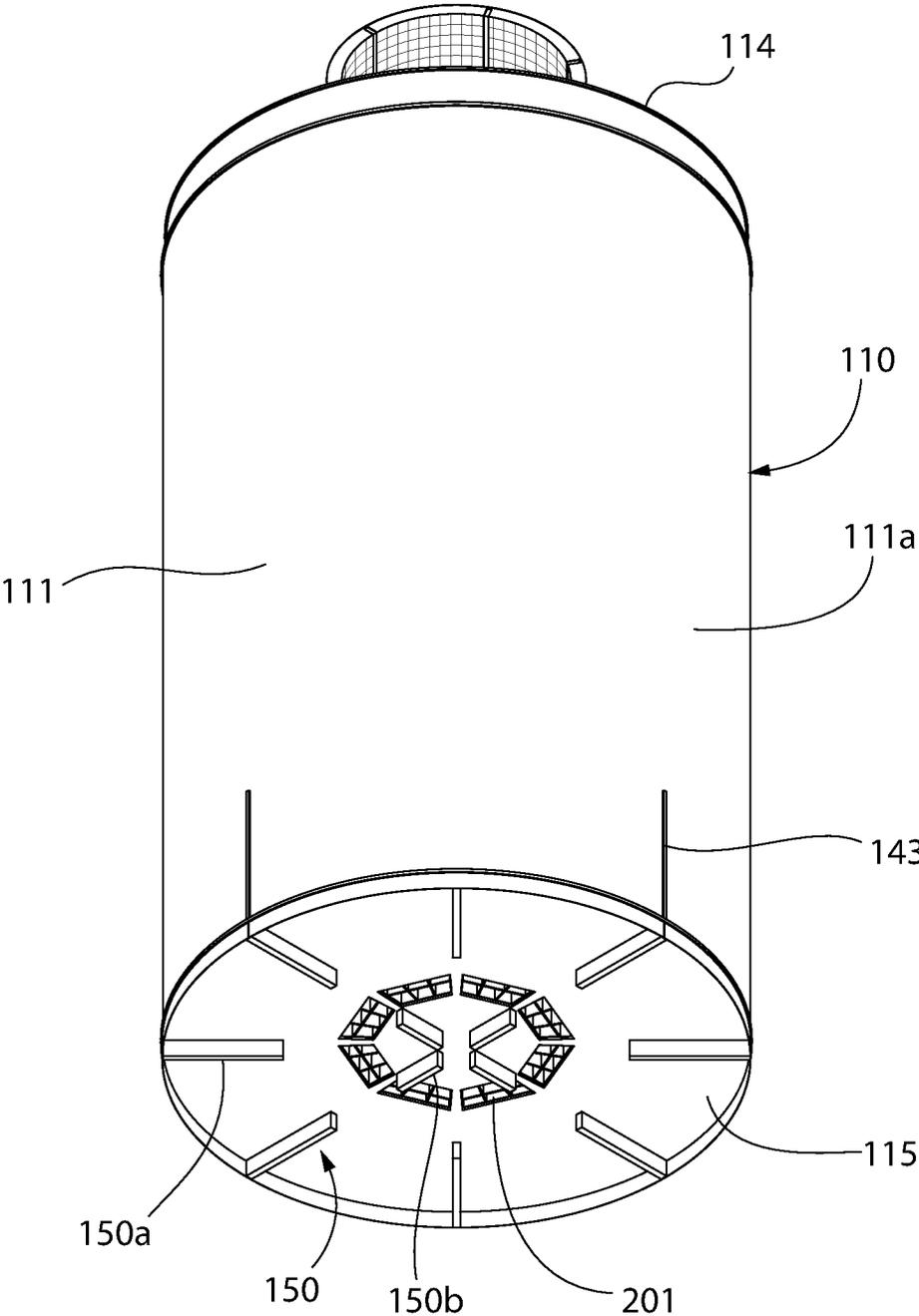


FIG. 2

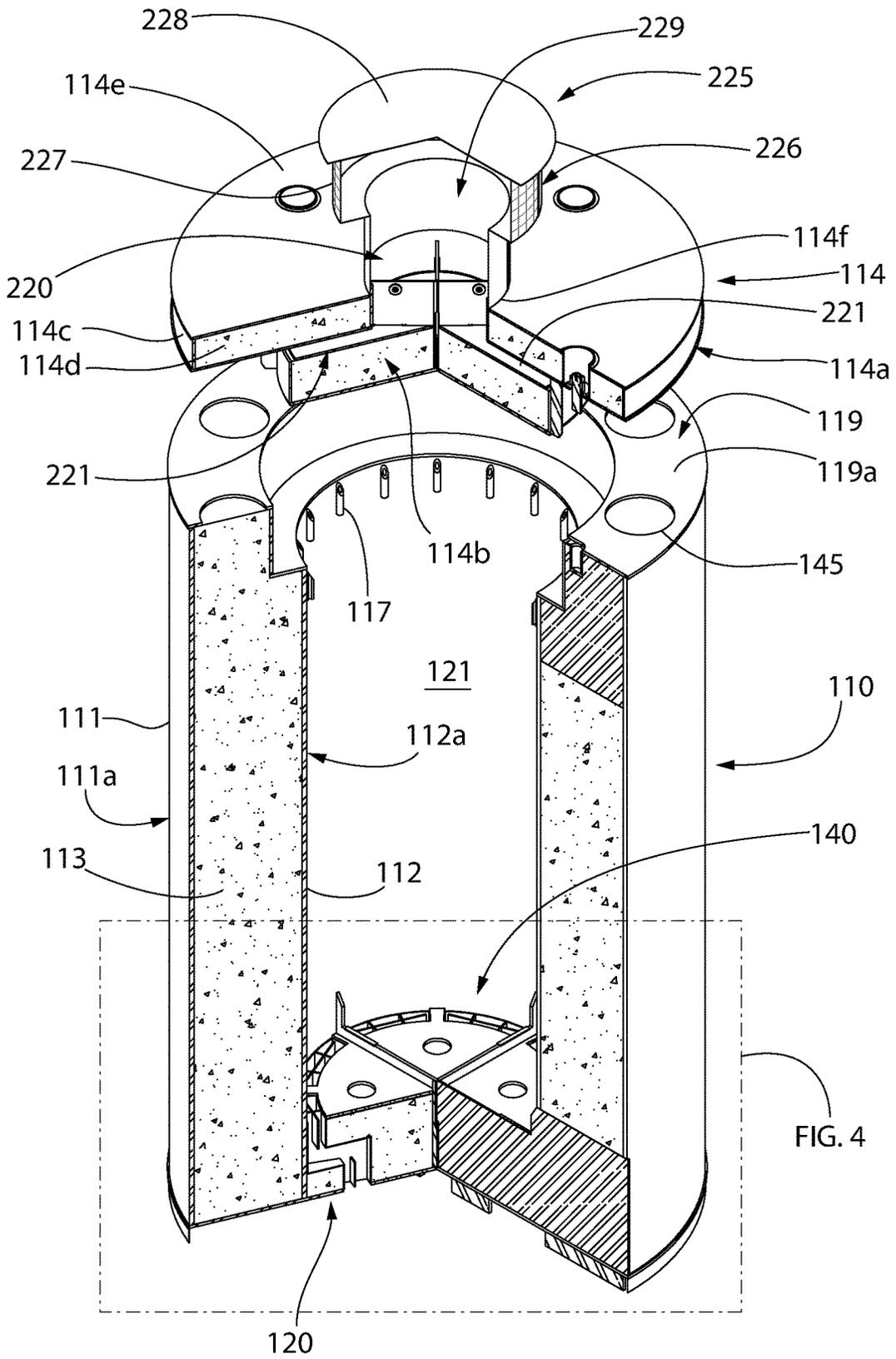


FIG. 3

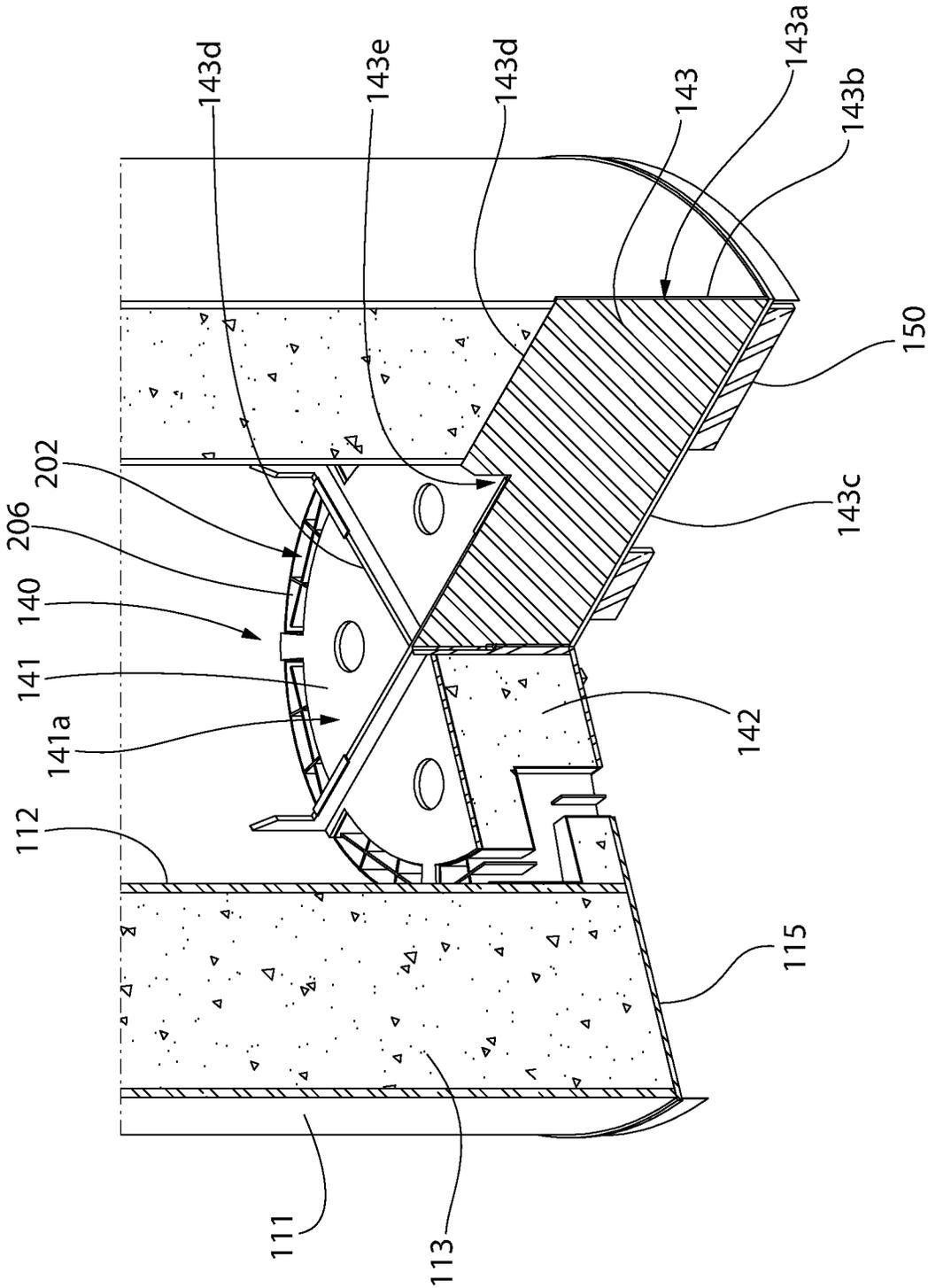


FIG. 4

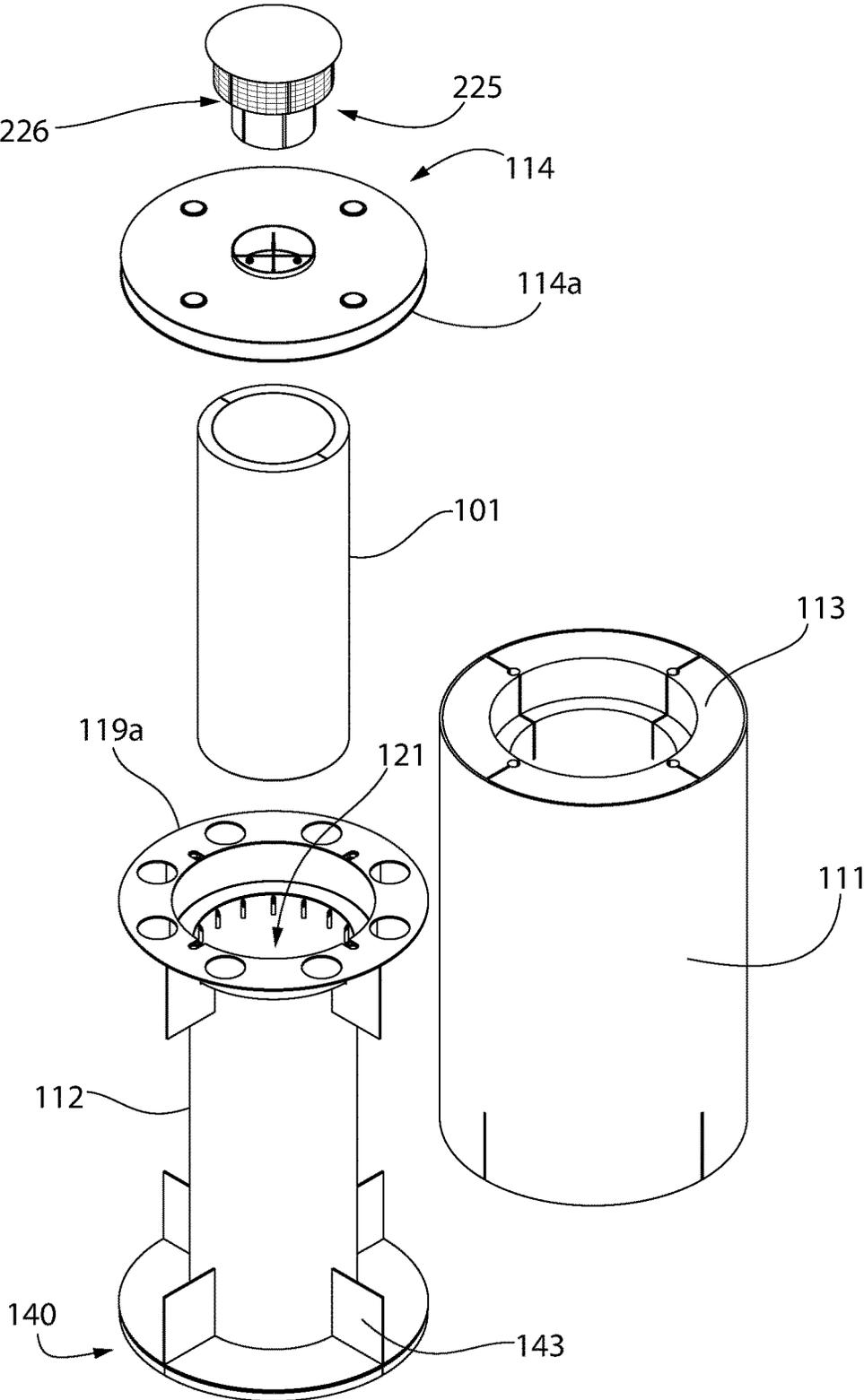


FIG. 6

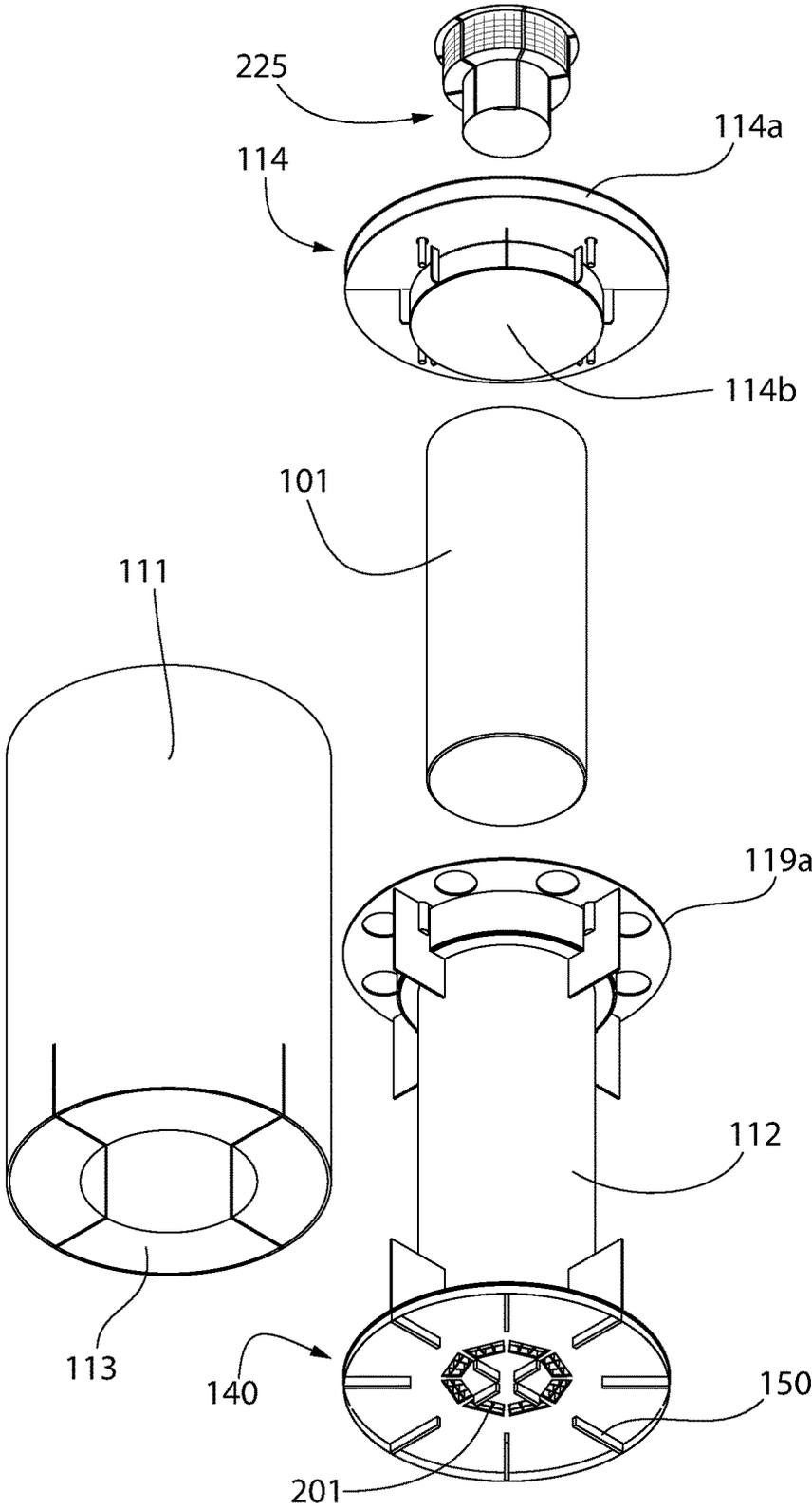


FIG. 7

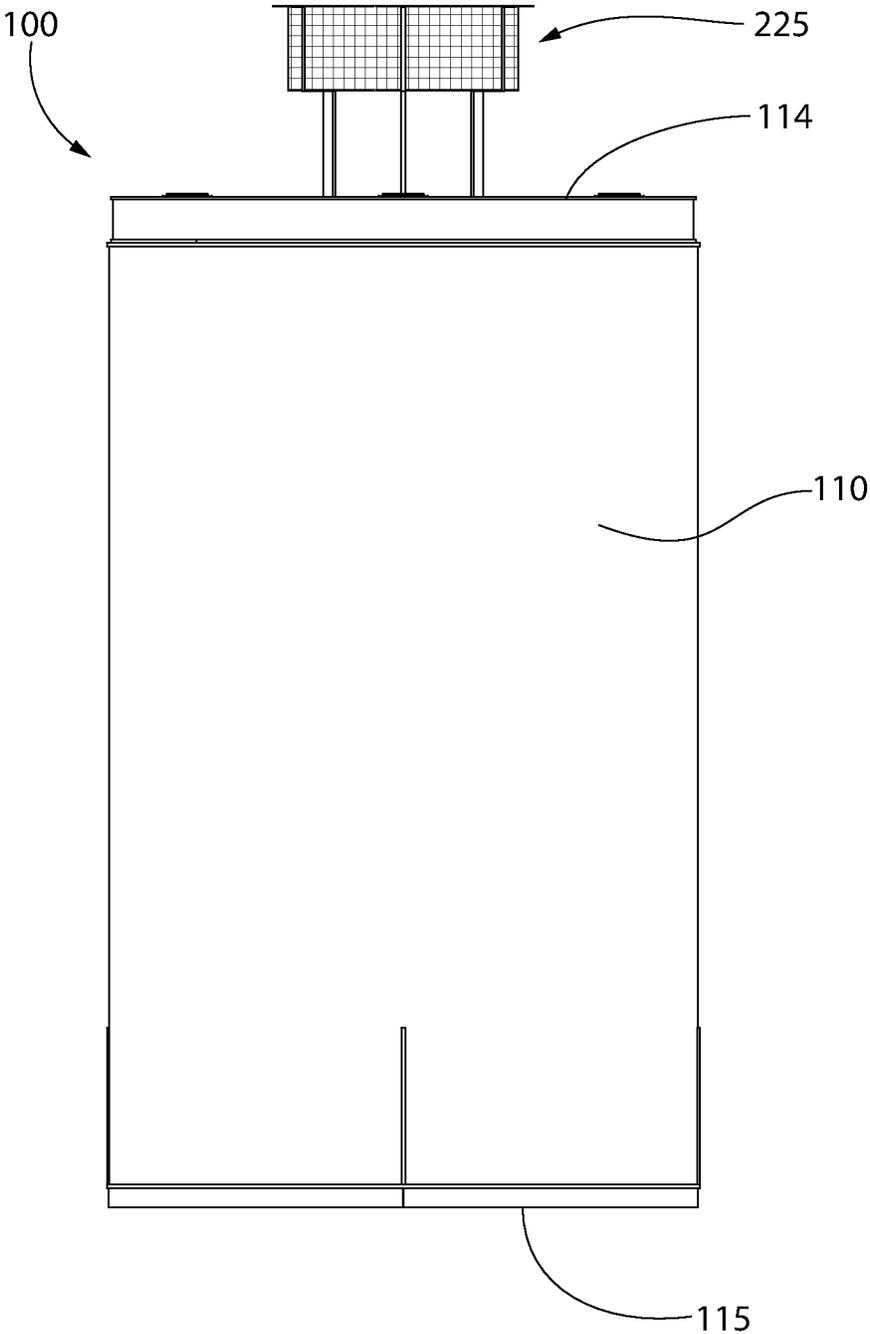


FIG. 8

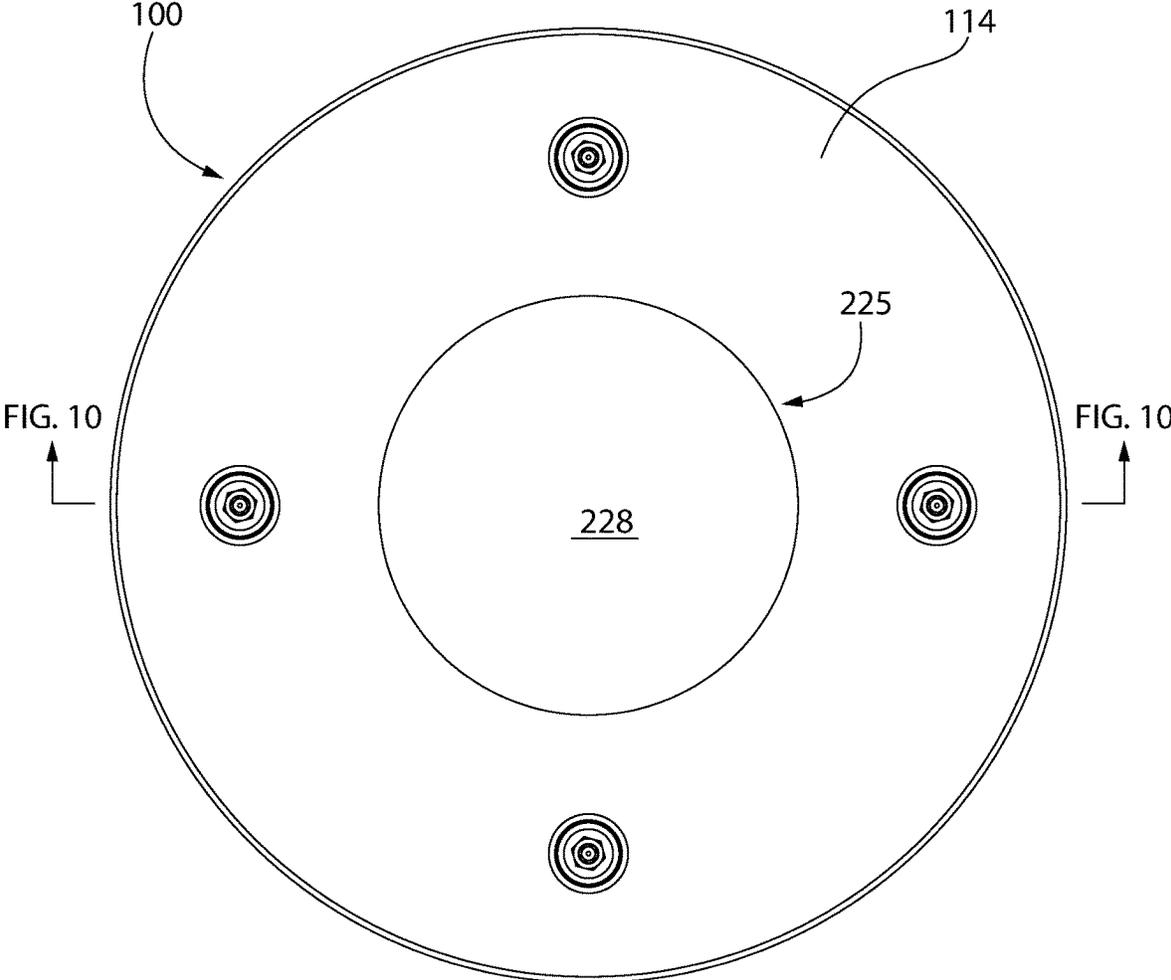


FIG. 9

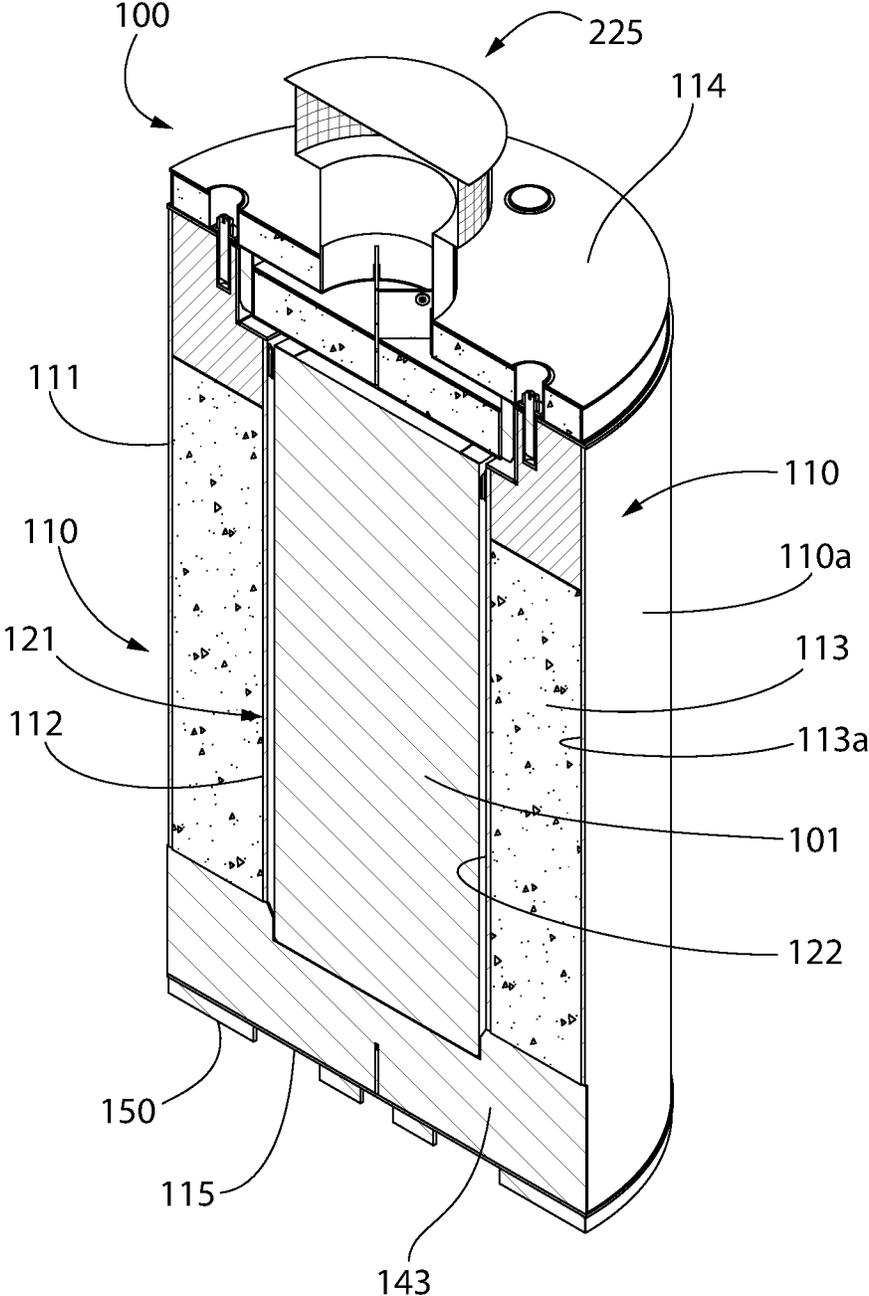


FIG. 10

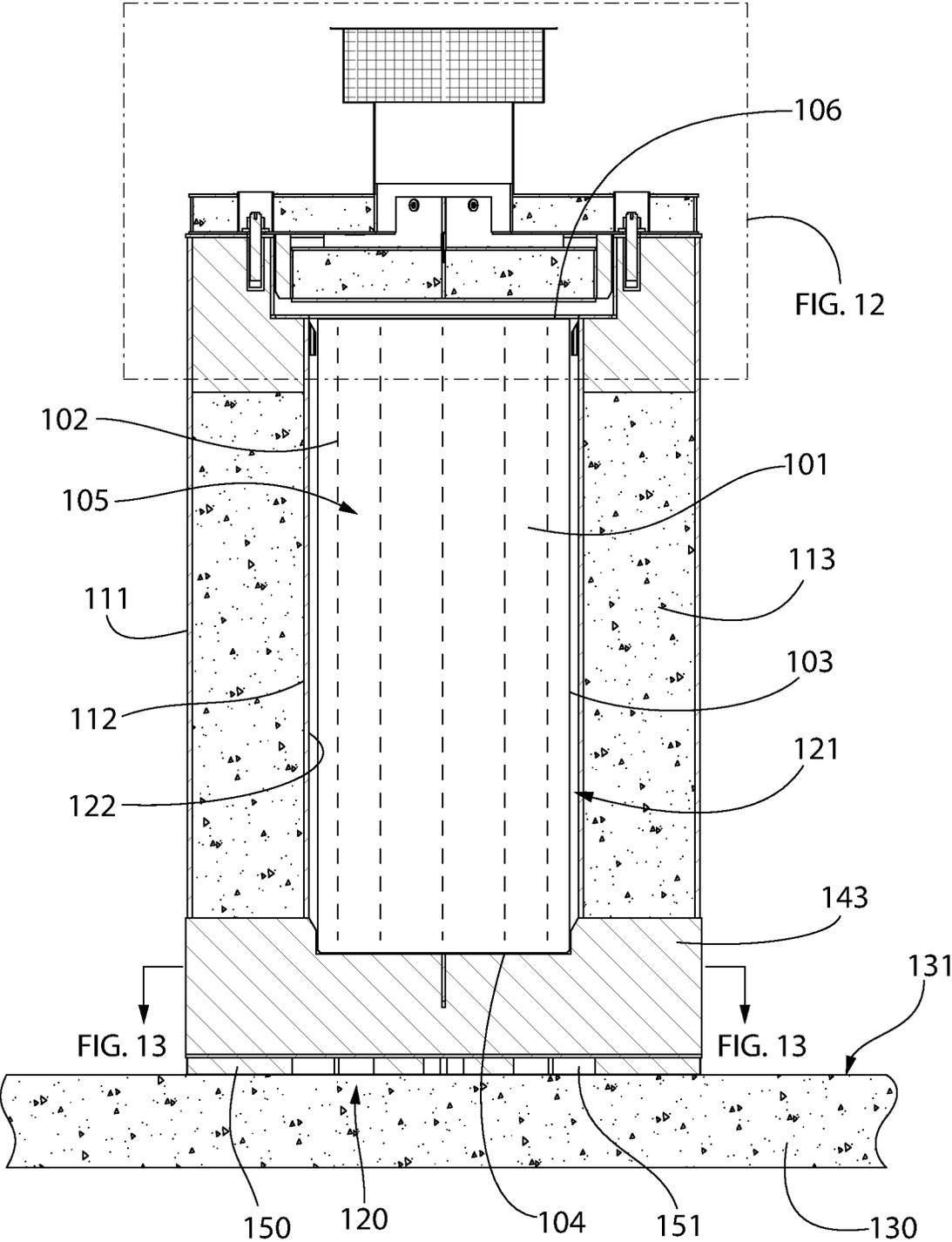


FIG. 11

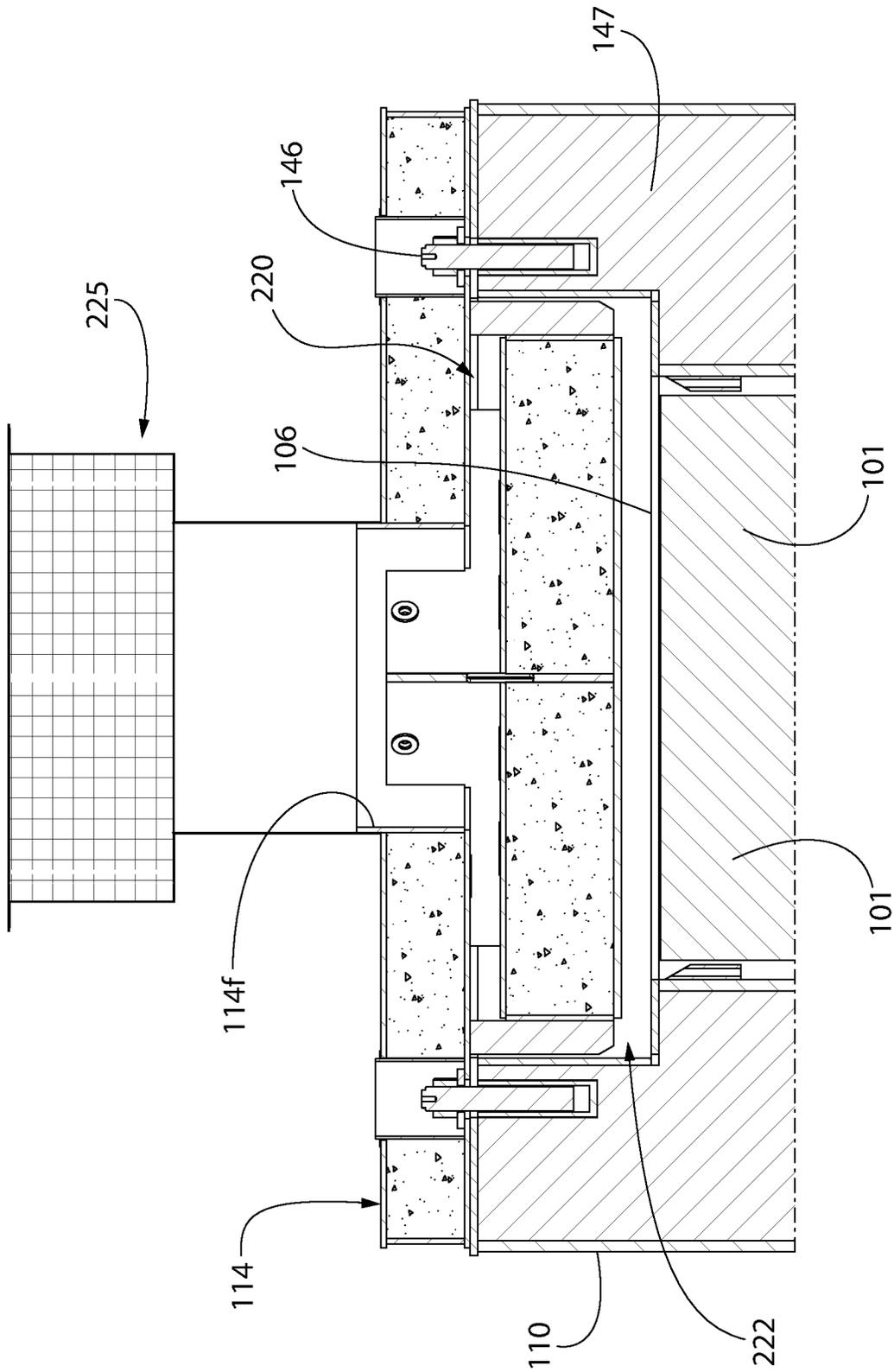


FIG. 12

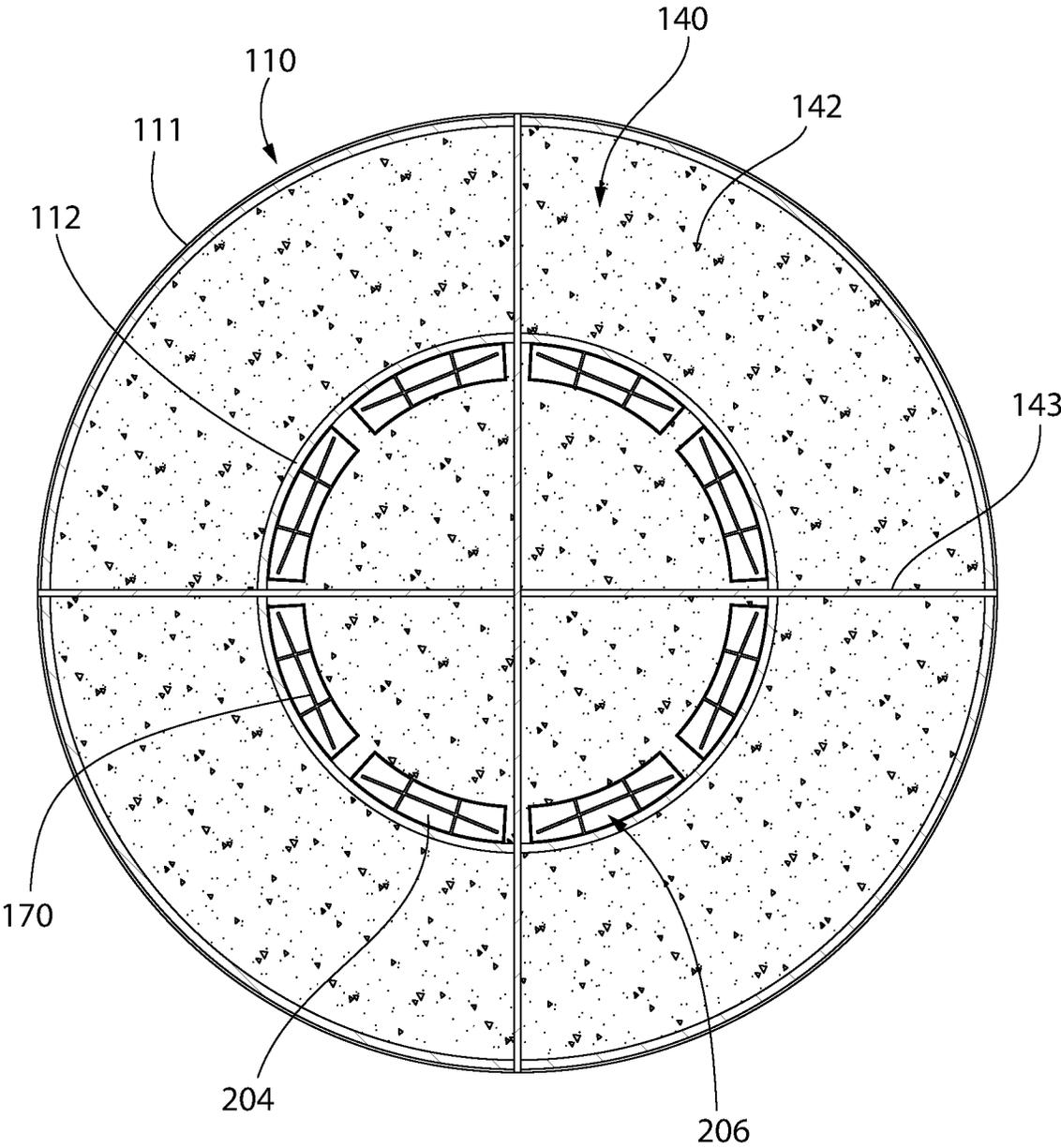


FIG. 13

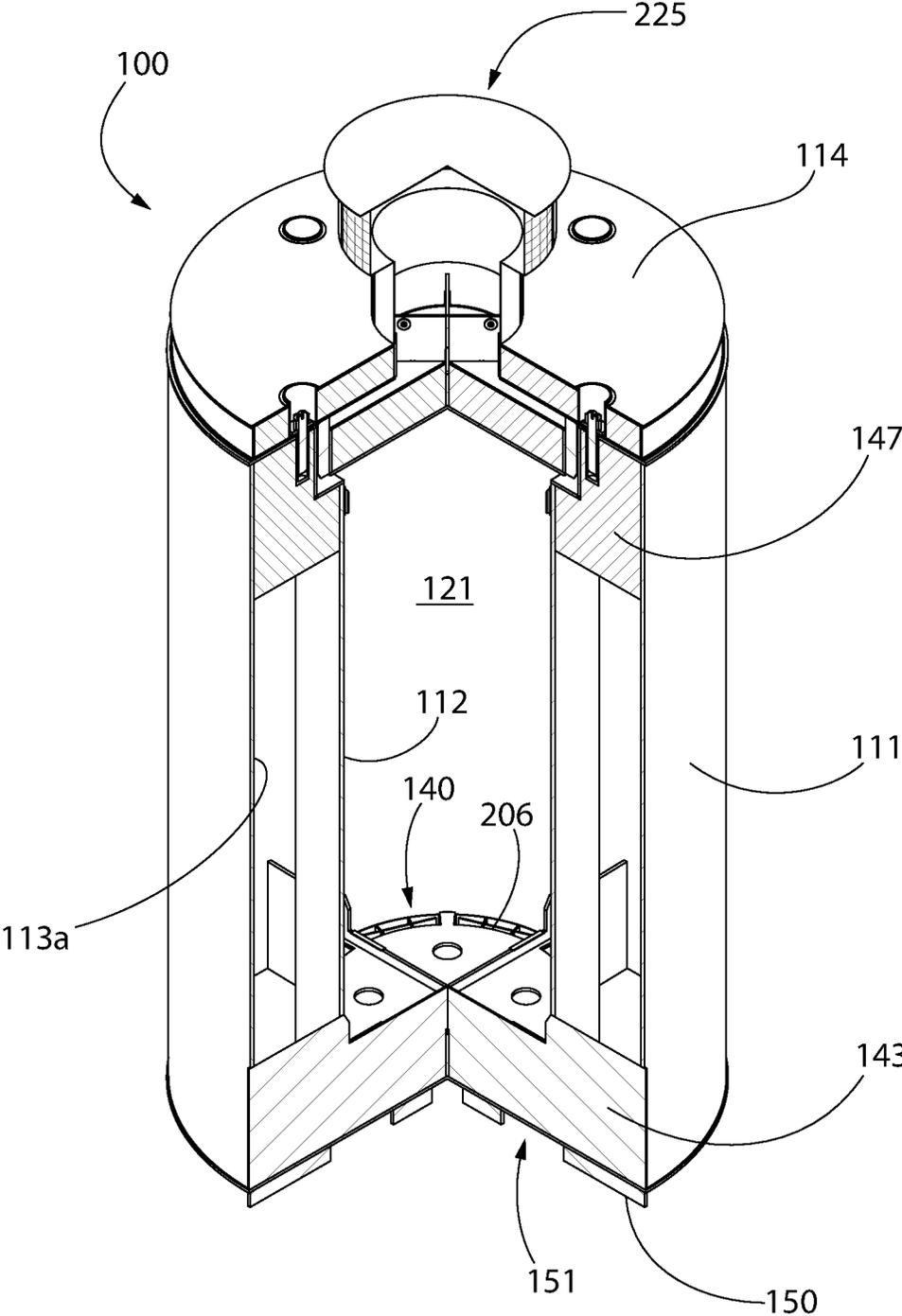


FIG. 14

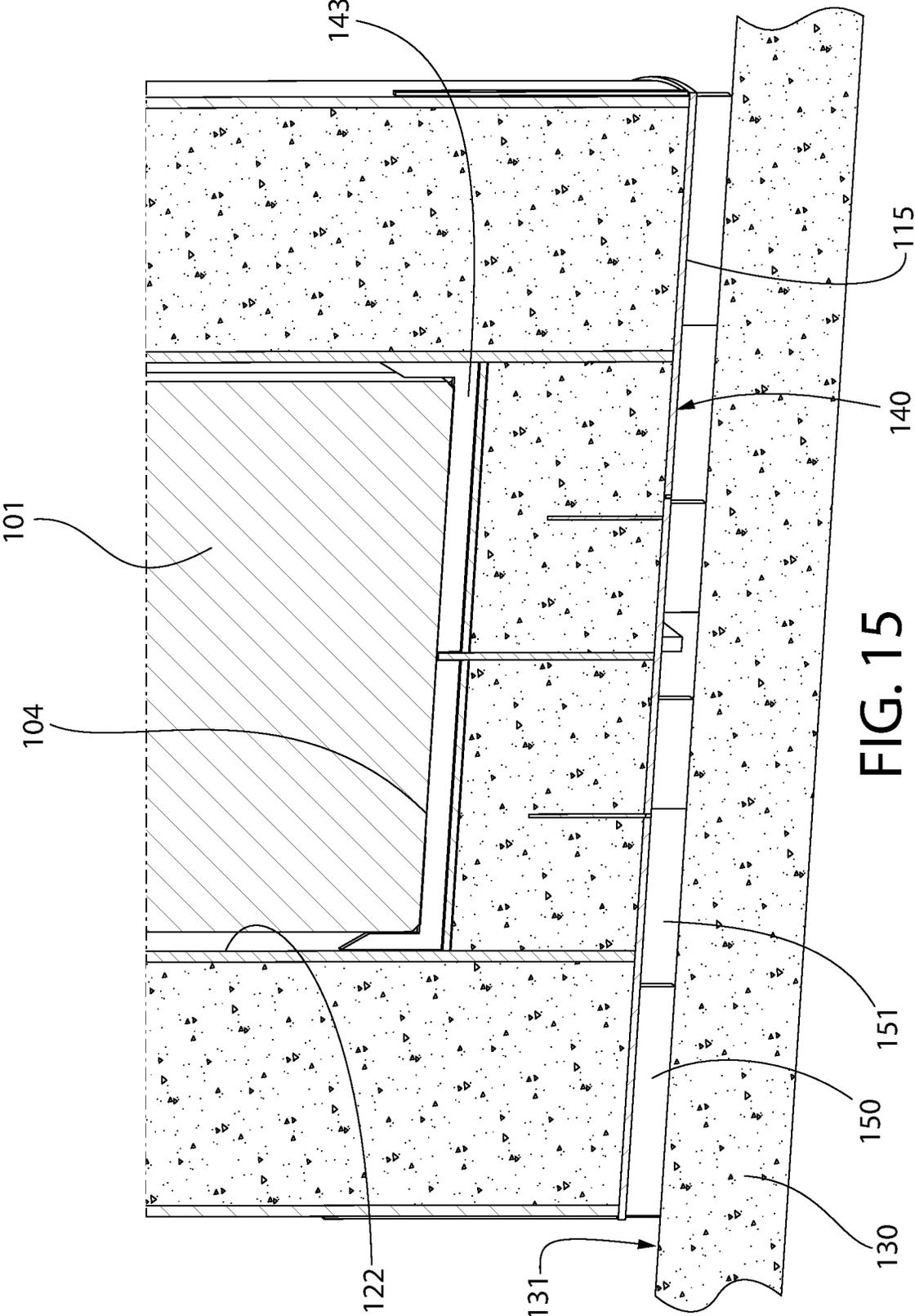


FIG. 15

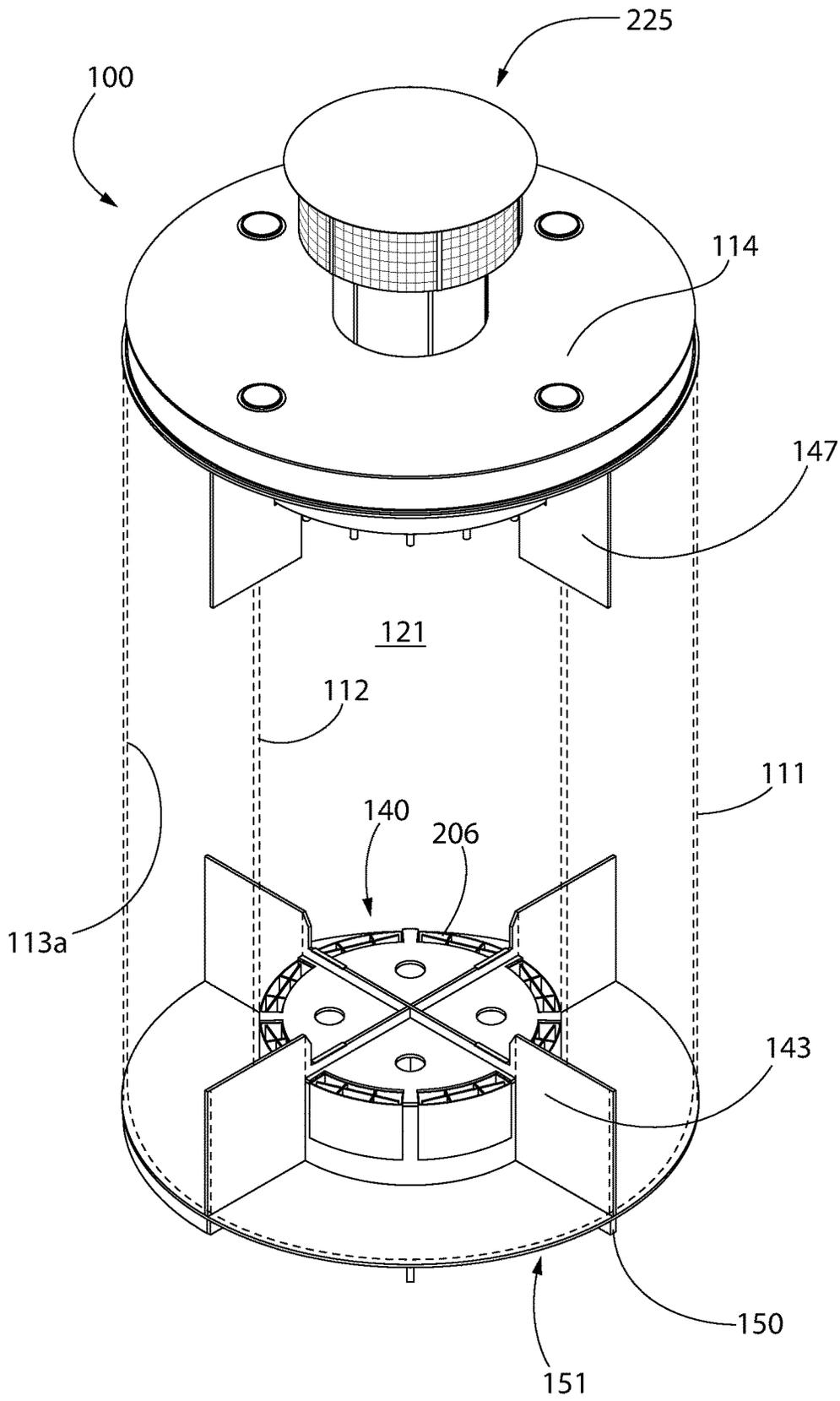


FIG. 16

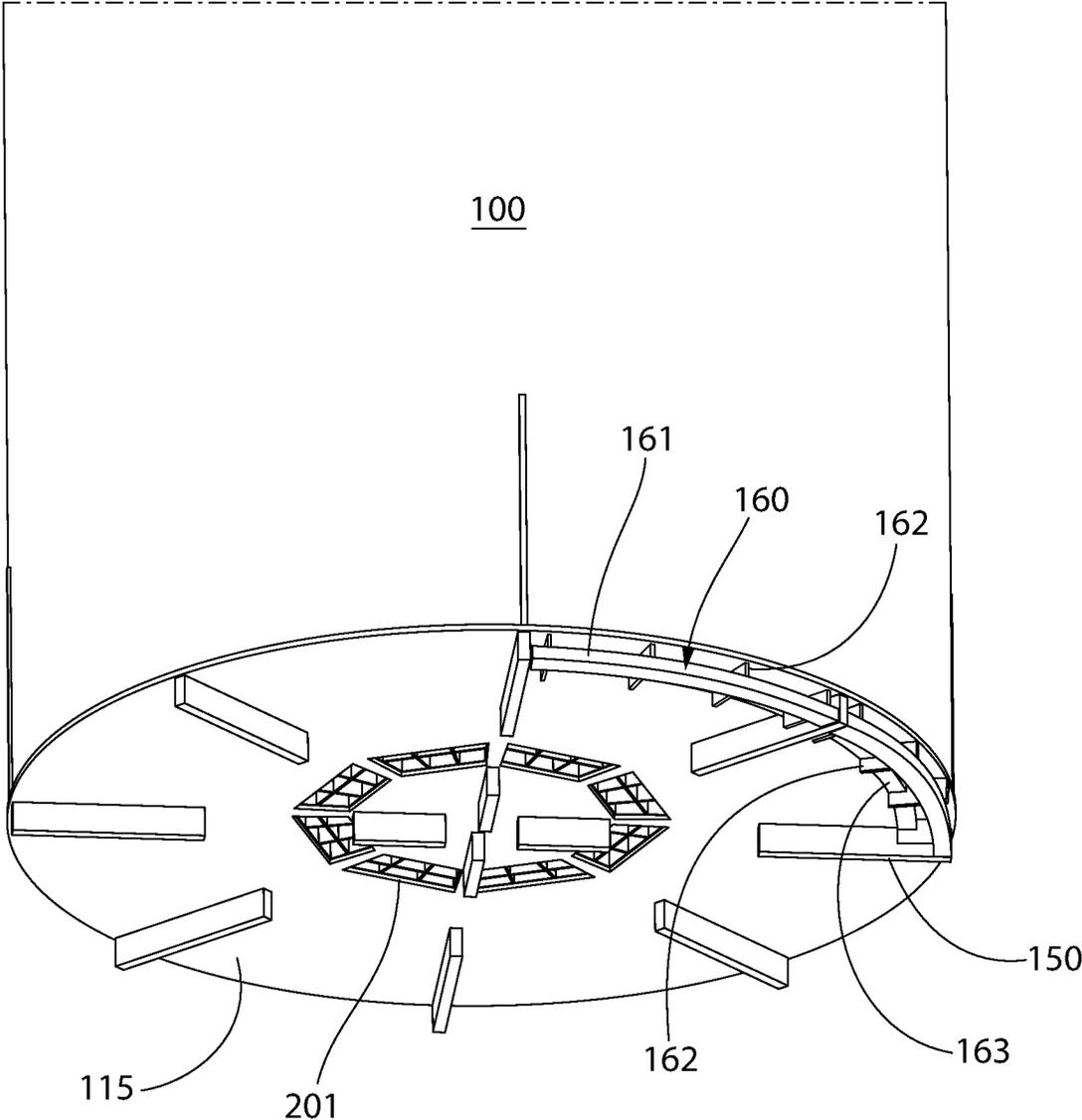


FIG. 17

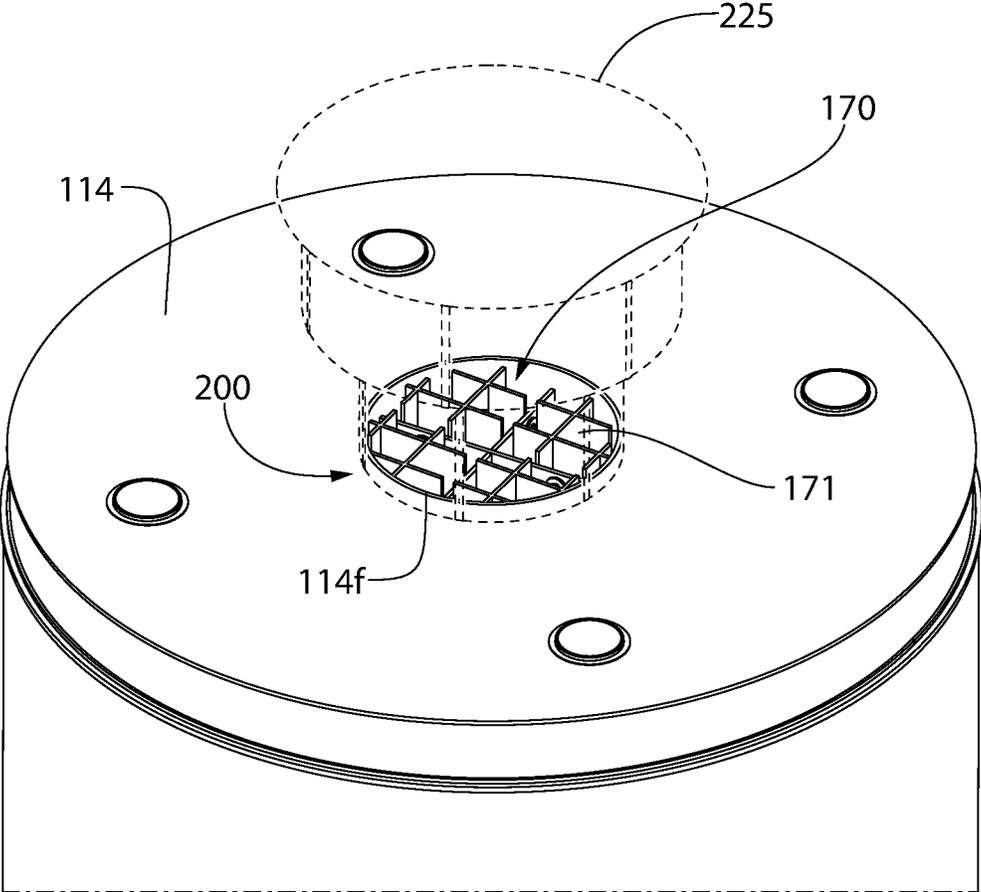


FIG. 18

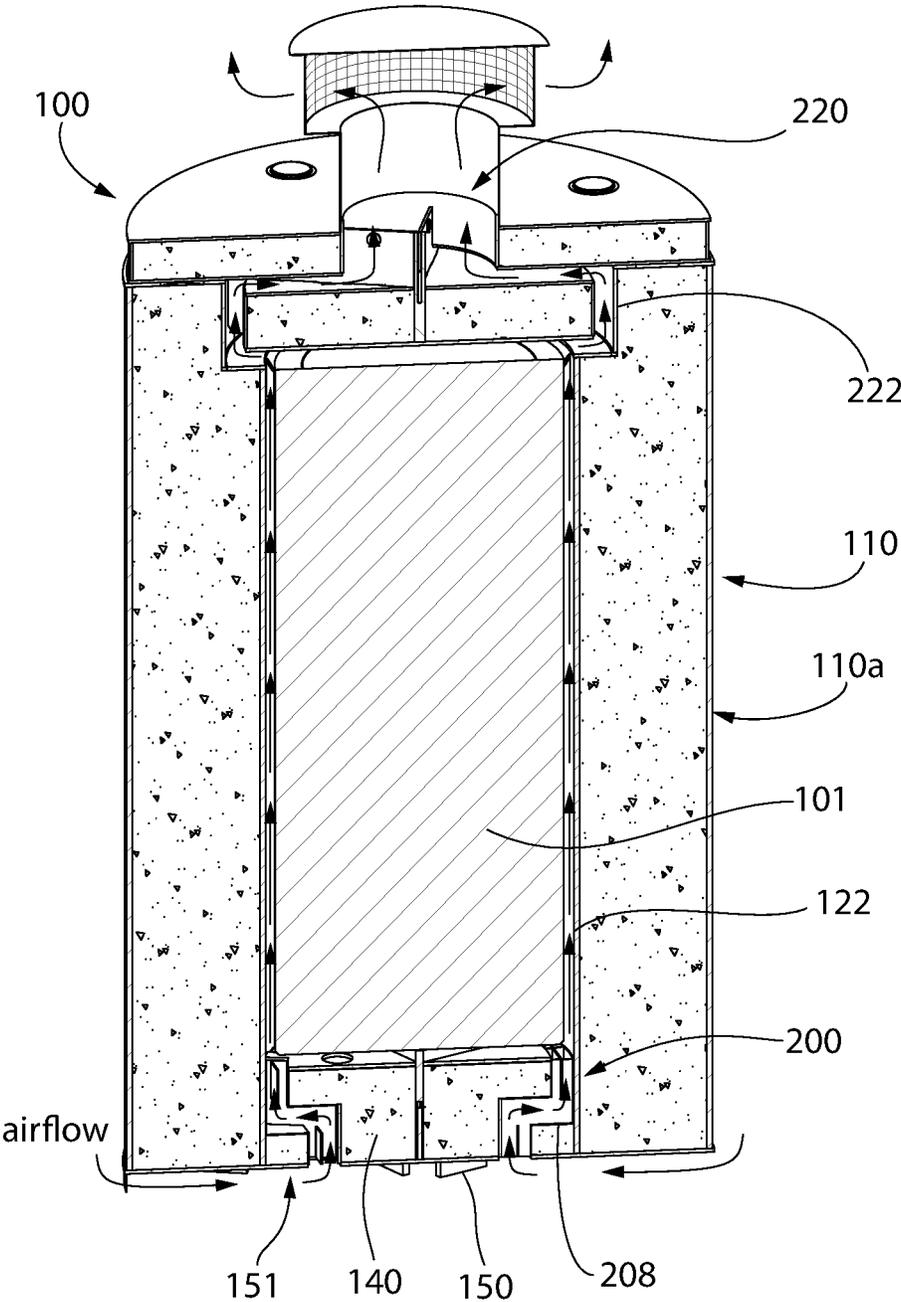


FIG. 19

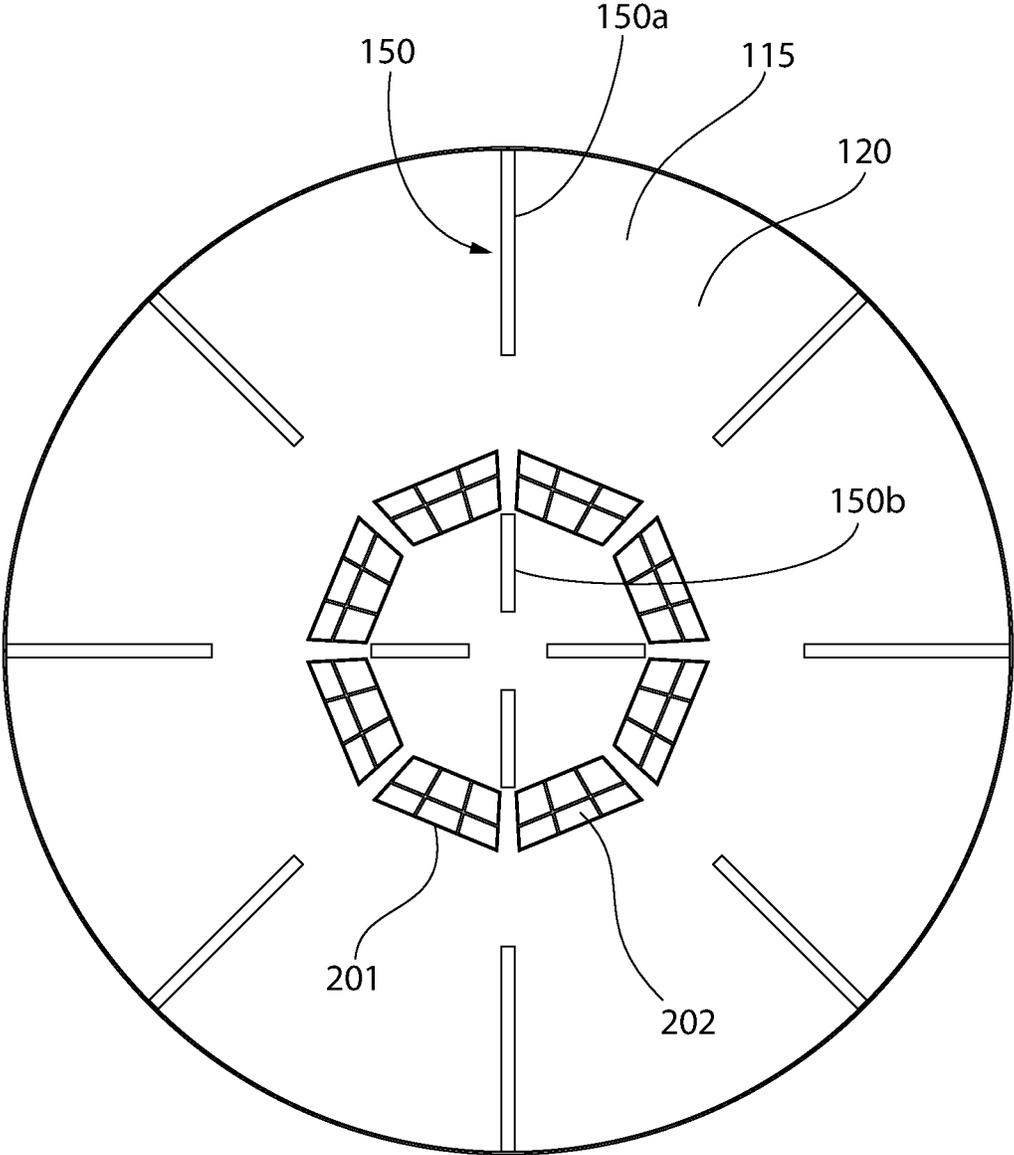


FIG. 20

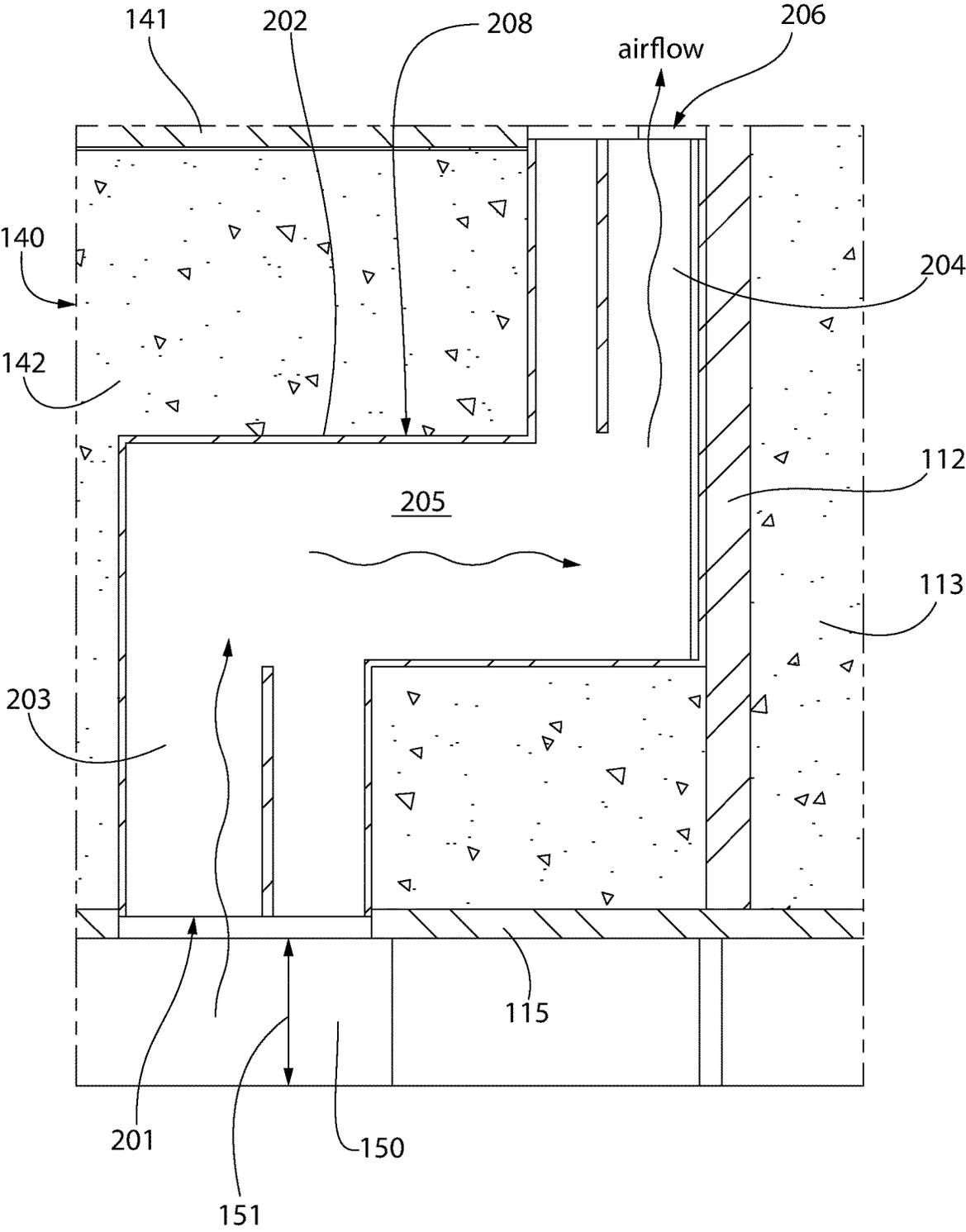


FIG. 21

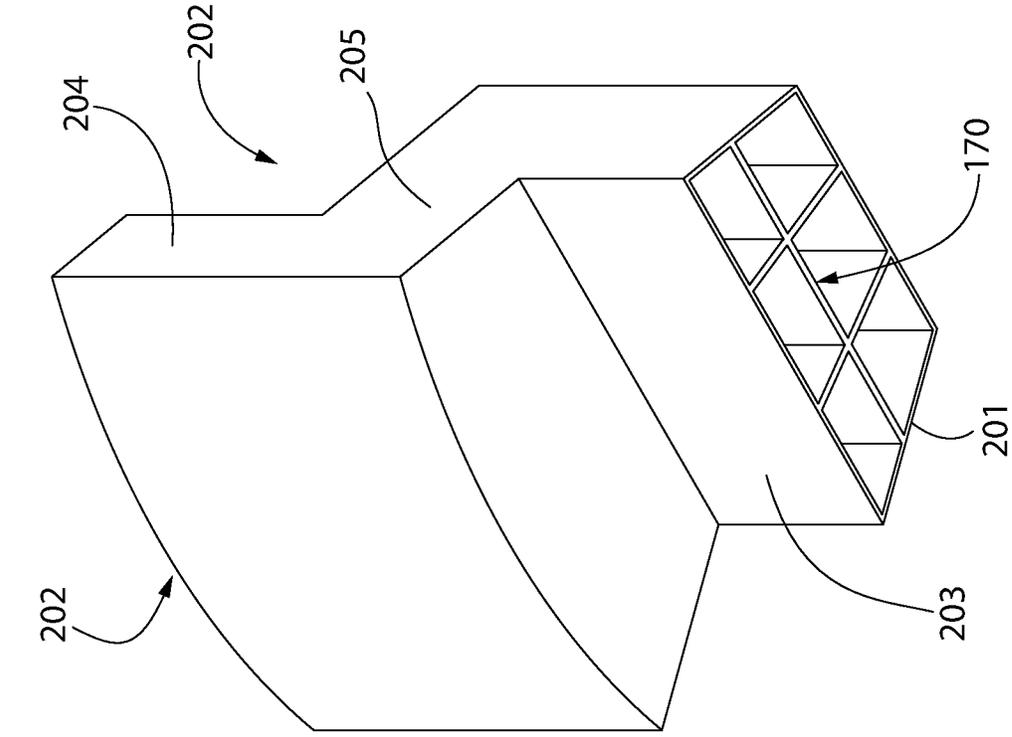


FIG. 22

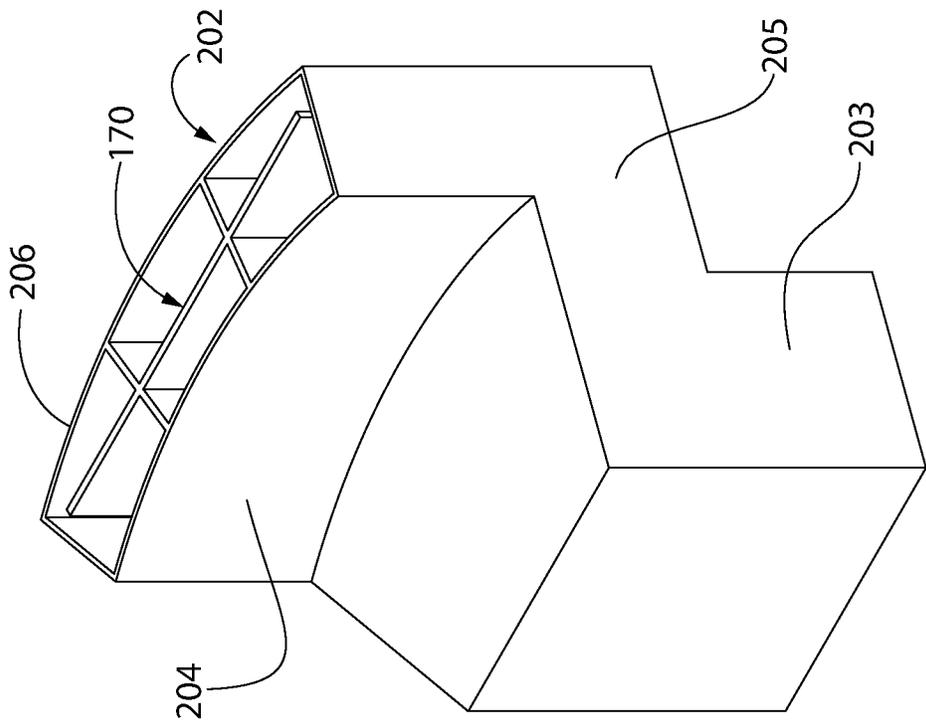


FIG. 23

VENTILATED CASK FOR NUCLEAR WASTE STORAGE**CROSS-REFERENCE TO RELATED APPLICATIONS**

The present application is a continuation of U.S. patent application Ser. No. 17/470,053 filed Sep. 9, 2021, which claims the benefit of U.S. Provisional Application No. 63/211,234 filed Jun. 16, 2021 and U.S. Provisional Application No. 63/223,578 filed Jul. 20, 2021; which are all incorporated herein by reference in their entireties.

BACKGROUND

The present invention relates generally to ventilated overpacks or casks used for dry storage and/or transport of high level nuclear waste from nuclear power generating plants or other nuclear facilities.

In the operation of nuclear reactors, the nuclear energy source is typically in the form of a plurality of hollow Zircaloy tubes each filled with enriched uranium pellets, which are collectively arranged in assemblages referred to as fuel assemblies. When the energy in the fuel assembly has been depleted to a certain predetermined level, the fuel assembly is removed from the nuclear reactor and referred to as used or spent nuclear fuel ("SNF"). The standard structure used to package or store the SNF assemblies discharged from light water reactors for off-site shipment or on-site dry storage is an all-welded stainless steel container. Such containers are well known and may be variously referred to as multi-purpose canisters (MPCs) such as those available from Holtec International of Camden, New Jersey, or dry storage canisters (DSCs).

Regardless of their name, these SNF canisters are characterized by a relatively thin-walled stainless shell to effectively transmit heat emitted by the decaying the SNF assemblies across the canister's wall boundary. The stainless steel shell has several full through-thickness continuous seam welds, including longitudinal seam welds and girth welds such as those that connect the shell to the top and bottom end closure plates. A fuel basket is typically arranged inside a metallic storage canister which defines an array of prismatic-shaped storage cells each of which is sized to hold a single fuel assembly, which in turn comprises a plurality of individual spent nuclear fuel rods.

A single canister is in turn stored and enclosed inside its own outer vertically ventilated module referred to as an overpack or cask. The casks are heavy radiation shielded vessels which block gamma and neutron radiation emitted from the SNF assemblies which passes through the canister shell and end plates. The ventilated casks are used for safe transport and/or storage of the multiple spent fuel assemblies within the inner fuel basket.

In addition to emitting neutron and gamma radiation requiring protective shielding, the highly radioactive SNF in the fuel assemblies (or other high level nuclear waste which may be stored in the waste canister) still produces considerable heat which must be dissipated to avoid damage to the fuel assemblies and spent fuel cladding stored in the canister. Ventilated casks use available ambient ventilation air to cool the canister and remove the heat emitted therefrom to protect the fuel assembly. Some casks have lateral ventilation openings in the sides and/or the lids which can create a path for radiation streaming to the ambient environment in some cases.

Improvements in ventilated casks used to store high level nuclear waste are therefore desired.

BRIEF SUMMARY

An improved nuclear waste storage system comprising a radiation-shielded ventilated cask for storing a nuclear fuel canister therein is provided. In one embodiment, the lateral side surfaces of the cask body does not have penetrations or openings for air ventilation, which eliminates any potential lateral or radial streaming paths for radiation emanating from the spent nuclear fuel (SNF) or other high level radioactive waste stored inside the canister in the cask. To achieve this, the present cask in one embodiment comprises a unique concrete-filled canister support structure at bottom. This radiation-shielded bottom closure structure supports the canister and is configured with integral inlet ducts which draw ambient cooling air into the internal cavity of the cask through downwardly open air inlets in the bottom baseplate of the canister support structure via a natural convective thermo-siphon flow effect. The canister support structure is configured to elevate and space the baseplate and concomitantly the cask above the concrete base pad on which the cask is positioned during use. This allows the cooling air to be drawn radially/horizontally inwards beneath the cask and then flow upwards through the air inlet in a vertical axial direction parallel to the vertical longitudinal or centerline axis of the cask. An air inlet plenum is formed between the base pad and baseplate of the cask.

Cooling air drawn into the cask continues to rise upward in a ventilation annulus formed in the internal cavity between the cask body and canister as the air is heated by the hot canister. The heated air is returned back to the ambient environment through air outlet ducts integrally formed in the radiation-shielded top lid of the cask. The lid is mounted on the cask body and configured such that there is no macro-path for leakage of radiation in the lateral or radial direction to the environment. The cask is configured for above-grade mounting in one embodiment so that ambient cooling air can readily reach the air inlet plenum from 360 degrees around the cask and becomes mixed before entering the cask. This plenum nullifies any pressure differentials surrounding the case cause by directional wind flow which enhance equal cooling of the entire canister inside the cask.

The downwardly open inlet ducts in the canister support structure are circuitously configured to eliminate any downwards straight line of sight through the ducts to prevent outward straight line radiation streaming from inside the cask. In one non-limiting embodiment, the air inlet ducts may have a generally Z-shaped transverse cross-sectional shape. In the unlikely event any radiation stream path were to occur, the straight-line radiation streaming would still be directed downwards from the air inlet towards the thick concrete base pad on which the cask is seated rather than in a radial or lateral direction where nuclear storage site workers might be present or near a boundary or fenced perimeter of the nuclear waste storage facility. The concrete base pad and soil below on which the pads rest are effective radiation shielding materials which act to block or absorb any escaping downwardly-directed radiation streaming.

The air outlet ducts in the cask lid are structured and circuitously configured as well to eliminate both upwards straight line radiation streaming and any laterally open air outlet penetrations in the side of the lid. Instead, the heated air is discharged back to atmosphere through the top of the lid via a protective cap structure.

3

In one aspect, a passively ventilated nuclear waste storage cask comprises: an elongated cask body defining a top, a bottom, a sidewall, and an internal cavity extending between the top and bottom along a vertical centerline axis of the cask, the internal cavity being configured for holding a nuclear waste storage canister; a lid attached to the top of the cask body; an air outlet formed in the lid; a downwardly open air inlet formed in the bottom of the cask body in fluid communication with the internal cavity and ambient atmosphere; and a canister support structure configured to support the canister in the internal cavity and engage a base pad, the canister support structure further configured elevate the bottom of the cask body above the base pad; wherein ambient cooling air is drawn in a flow path radially inwards beneath the bottom of the cask body and vertically upwards into the internal cavity through the air inlet.

According to another aspect, a passively ventilated nuclear waste storage system comprises: an elongated cask defining a top, a bottom, a sidewall, and an internal cavity extending between the top and bottom along a vertical centerline axis of the cask; a canister configured for holding nuclear waste, the canister positioned in the internal cavity of the cask and forming a circumferentially-extending ventilation annulus between the canister and cask; a lid attached to the top of the cask and comprising an air outlet in fluid communication with the internal cavity and ambient atmosphere; a concrete filled canister support structure disposed at the bottom of the cask and supporting the canister; a plurality of standoff members protruding downwards from the canister support structure which support and elevate the bottom of the cask from a base pad to form an air inlet plenum in fluid communication with ambient air; and air inlet ductwork formed through the canister support structure and in fluid communication with the ventilation annulus and air inlet plenum; wherein the air inlet ductwork is configured to draw ambient cooling air radially inwards into the air inlet plenum and the ventilation annulus via natural thermosiphon effect driven by heat emitted from the canister.

According to another aspect, a method for operating a passively ventilated nuclear fuel storage system comprises: providing a cask comprising an internal cavity and an ambient air ventilation system in fluid communication with the internal cavity and atmosphere; inserting a canister containing nuclear waste emitting heat into the internal cavity of a cask and onto a canister support structure fixedly coupled to the cask; drawing ambient cooling air into an air inlet plenum formed beneath the cask; flowing the cooling air upwards from the air inlet plenum through the canister support structure into the internal cavity of the cask; heating the cooling air in the internal cavity of the cask; and discharging the heated cooling air to atmosphere through a lid coupled to a top of the cask.

BRIEF DESCRIPTION OF THE DRAWINGS

The present invention will become more fully understood from the detailed description and the accompanying drawings, wherein like elements are labeled similarly and in which:

FIG. 1 is a top perspective view of a passively ventilated cask with for storing high level nuclear radioactive waste material such as spent nuclear fuel;

FIG. 2 is a bottom perspective view thereof;

FIG. 3 is a vertical partial cross-sectional perspective view thereof;

FIG. 4 is an enlarged detail taken from FIG. 3;

4

FIG. 5 is a top perspective view of a bottom canister support structure of the cask;

FIG. 6 is a top exploded perspective view of the cask;

FIG. 7 is a bottom exploded perspective view of the cask;

FIG. 8 is a side view of the cask;

FIG. 9 is a top view of the cask;

FIG. 10 is a full vertical cross-sectional perspective view of the cask;

FIG. 11 is a full vertical side cross-sectional perspective view of the cask;

FIG. 12 is a partial vertical cross-sectional view of the upper portion of the cask and lid;

FIG. 13 is a transverse/horizontal cross sectional view of the canister support structure of the cask;

FIG. 14 is a vertical partial cross-sectional perspective view of the of the cask with concrete liner of the sidewall not shown;

FIG. 15 is a vertical partial cross-sectional view of the lower portion of the cask and concrete base pad supporting the cask;

FIG. 16 is a vertical partial cross-sectional perspective view of the of the cask with concrete liner of the sidewall and bottom canister support structure not shown;

FIG. 17 is a bottom perspective view of the bottom of the cask showing installed curved radiation photon scattering attenuators;

FIG. 18 is a top perspective view of the upper portion of the cask showing a radiation photon scattering duct attenuator installed in the air outlet duct of the ambient air ventilation system of the cask;

FIG. 19 is another vertical cross-sectional view of the cask with a spent nuclear fuel canister positioned in the cask;

FIG. 20 is a bottom view of the cask;

FIG. 21 is an enlarged vertical cross sectional view of an air inlet duct of the canister support structure;

FIG. 22 is a top perspective view of the air inlet duct; and

FIG. 23 is a bottom perspective view of the air inlet duct.

All drawings are schematic and not necessarily to scale. Features shown numbered in certain figures are the same features which may appear un-numbered in other figures unless noted otherwise herein.

DETAILED DESCRIPTION

The features and benefits of the invention are illustrated and described herein by reference to exemplary embodiments. This description of exemplary embodiments is intended to be read in connection with the accompanying drawings, which are to be considered part of the entire written description. Accordingly, the disclosure expressly should not be limited to such exemplary embodiments illustrating some possible non-limiting combination of features that may exist alone or in other combinations of features.

In the description of embodiments disclosed herein, any reference to direction or orientation is merely intended for convenience of description and is not intended in any way to limit the scope of the present invention. Relative terms such as "lower," "upper," "horizontal," "vertical," "above," "below," "up," "down," "top" and "bottom" as well as derivatives thereof (e.g., "horizontally," "downwardly," "upwardly," etc.) should be construed to refer to the orientation as then described or as shown in the drawing under discussion. These relative terms are for convenience of description only and do not require that the apparatus be constructed or operated in a particular orientation. Terms such as "attached," "affixed," "connected," "coupled,"

5

“interconnected,” and similar refer to a relationship wherein structures are secured or attached to one another either directly or indirectly through intervening structures, as well as both movable or rigid attachments or relationships, unless expressly described otherwise.

As used throughout, any ranges disclosed herein are used as shorthand for describing each and every value that is within the range. Any value within the range can be selected as the terminus of the range. In addition, all references cited herein are hereby incorporated by reference in their entireties. In the event of a conflict in a definition in the present disclosure and that of a cited reference, the present disclosure controls.

FIGS. 1-23 depict various aspects and components of a nuclear waste storage system comprising a first embodiment of a passively cooled and naturally ventilated outer nuclear waste storage module or cask **100** configured for holding a nuclear waste canister **101** which contains spent nuclear fuel (SNF) or other high level radioactive waste materials. Cask **100** is constructed and configured for above grade placement in one embodiment such as on a top surface **131** of a flat reinforced concrete base pad **130** slab which may rest on soil or another structure. The cask may be anchored to the base pad if desired via fasteners to prevent shifting during a postulated seismic event or projectile impact.

Canister **101** is a vertically elongated and hermetically sealed (i.e. gas tight) vessel in one embodiment comprising cylindrical shell **103**, circular bottom closure plate **104** affixed to a bottom end of the shell, and a circular top closure plate **106** coupled to a top end of the shell. The top and bottom closure plates may be hermetically seal welded to the shell via circumferentially continuous girth seal welds at the weld seams. An interior space **105** is defined within the shell which is configured for holding the SNF fuel assemblies **102** (represented schematically in FIG. **11** by dashed lines) or other high level radioactive waste materials. Such fuel assemblies are well known in the art without further elaboration. For example, a typical rectangular fuel assembly for U.S. style pressurized water reactors (PWRs) is disclosed in commonly-owned U.S. patent application Ser. No. 17/115,005, which is incorporated herein by reference in its entirety. The fuel assemblies **102** contain the fuel rods or “cladding” with decaying uranium which generates considerable heat that must be dissipated to protect the structural integrity and containment of the fuel. This in turn heats the canister which emits the heat. The canister including shell **103** and the top and bottom closure plates **104**, **106** preferably may be made of stainless steel in one embodiment for corrosion protection.

Cask **100** may be a heavily radiation-shielded double-walled vessel in one embodiment including a vertically elongated cask body **110** formed by a cylindrical outer shell **111** and inner shell **112**, and radiation shielding material **113** disposed in an annular space **113a** formed therebetween. The shells **111**, **112** and shielding material **113** collectively define the sidewall **110a** of the cask. The inner and outer shells are concentrically arranged relative to each other as shown.

In one embodiment, the shielding material **113** of cask body **110** may comprise a high-density concrete mass or liner for neutron and gamma radiation blocking. The concrete in some embodiments may comprise hematite (iron oxide compound Fe_2O_3) and/or other iron-containing aggregates which substantially boost the thermal conductivity of the liners resulting in a significant increase in the rate of conductive heat transfer from the inside surface of the cask to the outside surface exposed to ambient atmosphere. Other radiation shielding materials may be used in addition to

6

and/or instead of concrete including lead for gamma radiation shielding, boron containing materials for neutron blocking (e.g. Metamic®, Holtite® or others), steel, and/or others shielding material typically used for such purposes in the art.

5 Inner shell **112** of the cask body **110** defines an interior or internal surface **112a** and outer shell **111** defines an exterior or external surface **111a** of the cask. Surfaces **111a**, **112a** formed by the shells may correspondingly be cylindrical and arcuately curved in one embodiment. The cask body further includes an open top **119** (when not closed by lid **114**) defined by the upper end of the cask body sidewall **110a** and bottom **120** defined by baseplate **115** at the lower end of the cask body sidewall.

The passively cooled and ventilated nuclear waste storage cask **100** may be vertically elongated and oriented when in use as shown in the illustrated embodiment. The inner and outer shells **112**, **111** may be formed of a suitable metallic material, such as without limitation steel (e.g. carbon or stainless steel). If carbon steel is used at least the exterior surface **111a** of the cask may be epoxy painted/coated for corrosion protection. The metal shells **111**, **112** may each have representative thickness of about $\frac{3}{4}$ inches as one non-limiting example; however, other suitable thicknesses may be used.

25 Cask **100** comprises a vertically-extending internal cavity **121** which extends along a vertical longitudinal or centerline axis CL defined by and passing through the geometric centerline of the elongated cask. Cavity **121** may be of cylindrical configuration in one embodiment with a circular cross-sectional shape; however, other shaped cavities with corresponding cross-sectional shapes may be used including polygonal shapes and other non-polygonal shapes (e.g. rectilinear, hexagon, octagonal, etc.).

35 Cask **100** further includes a radiation shielded canister support structure **140** disposed at the bottom **120** of the cask body **110** which essentially closes the bottom end of internal cavity **121** of the cask (except for the cooling air inlet structure further described herein to allow ambient ventilation air to enter the cavity at bottom). The canister support structure **140** is configured to support and elevate the canister **101** within the internal cavity of the cask in the manner shown. Canister support structure **140** has a composite construction which comprises lower and outermost baseplate **115**, upper top plate **141** facing and disposed inside the internal cavity **121** at bottom, peripheral cylindrical vertical shell **144** extending therebetween, and concrete liner **142** for enhanced radiation shielding filling the interior space created by the shell and the top and bottom plates. Top plate **141** and baseplate **115** may be circular and flat. Baseplate **115** projects radially outwards beyond the vertical shell **144** (see, e.g., FIGS. 4-5). The baseplate covers the entire bottom of cask body **110** and extends circumferentially along the entire bottom end of the outer shell **111** of the cask body at the perimeter of the cask. The baseplate **115**, top plate **141**, and vertical shell **144** of the canister support structure may be welded together to form a permanently joined assemblage. Multiple fill holes **145** are provided in top plate **141** to pour the concrete liner into each quadrant of the assemblage after welding which is defined by the canister support rib plates **143** of canister support structure **140** as further described herein.

65 Baseplate **115** may be hermetically seal welded to the bottom ends of the inner and outer shells **112**, **111** at the bottom **120** of the cask body and structurally supports the shells. Top plate **141** has a smaller diameter than baseplate **115** and is disposed and elevated inside the cask internal cavity **121** spaced upwards from the bottom of the cask. Top

plate **141** and baseplate **115** may each have a flat and circular configuration in one non-limiting embodiment as shown. The top plate includes a flat upward facing top surface **141a** which is exposed inside the cask internal cavity **121**. Baseplate **115**, top plate **141**, and shell **144** of canister support structure **140** may be made of a similar metallic material as the shells **111**, **112** (e.g., steel or stainless steel). In one embodiment, baseplate **115** may be about 3 inches thick. The bottom surface **115a** of baseplate **115** defines the bottom of the cask **100**.

The canister support structure **140** forms a pedestal for supporting canister **101** in cask internal cavity **121** and further comprises an assemblage of multiple intersecting canister support rib plates **143** which are an integral part of the support structure. In one embodiment, canister **101** is supported by and seated directly on the rib plates. Rib plates **143** are elongated in length and extend radially between opposing diametrically opposite portions of the sidewall **110a** of the cask body **110**. The rib plates are embedded in the sidewall **110a** (including concrete liner **113**) and have vertical outer ends **143a** which may be welded to outer shell **111** of the cask. Ends **143a** may protrude completely through complementary configured slots **143b** in the outer shell in one embodiment for additional structural support by the shell base material in addition to the weldments thereto.

The horizontal bottom edges **143c** of rib plates **143** may be welded to the top surface of the baseplate **115**. Rib plates **143** protrude upwards above the top surface **141a** of top plate **141** of the canister support structure such that their horizontal top edges **143d** are spaced apart above surface **141a** of the top plate to engage the bottom closure plate **104** of canister **101** seated thereon. This elevates the canister and forms a gap or space between canister bottom closure plate **104** and top surface **141a** of top plate **141** which allows heat emitted from the bottom of canister **101** to be drawn away by the ambient cooling air flowing through internal cavity **121** of the cask **100**.

Rib plates **143** in one embodiment may further include a stepped shoulder **143a** formed in top edge **143d** of the plates adjacent inner shell **112** inside the cask internal cavity **121**. Shoulders **143a** engage the sides of the canister shell **103** to center and stabilize the canister in the cask during transport and in the case of a seismic event. In one embodiment, the shoulders **143a** are preferably configured to space the canister shell **103** apart from the inner surface **112a** of the cask inner shell **112** such that a substantially uniform ventilation annulus **122** (further described herein) is maintained between the cask **100** and canister when the canister is positioned in internal cavity **121** of the cask.

In one embodiment, rib plates **143** may be arranged in an "X" shaped intersecting pattern as shown. The intersection of the plates **143** may fall on the vertical longitudinal or centerline axis CL of the cask. Rib plates **143** may be welded to each other at the intersection in some embodiments. Such an intersecting arrangement strengthens the rib assemblage particularly since the central portion of rib plates **143** are embedded in the concrete liner **142** of the canister support structure **140** (see, e.g., FIG. 5).

Cavity **121** of cask **100** has a configuration in transverse cross-sectional area (perpendicular to centerline axis CL) and height suitable for holding a single SNF canister **101** therein which holds the SNF assemblies or other high level radioactive waste. The internal diameter of cask cavity **121** is intentionally larger than the diameter of the fuel canister **101** to form a ventilation annulus **122** between the canister **101** and inner shell **112** when the canister is emplaced in the cask. The radial width of annulus **122** preferably is sufficient

to draw heat generated by the nuclear waste within the canister away from the canister as the cooling ventilation air flowing upwards alongside the canister. The upward flow of cooling air in the annulus is automatically driven via a natural convective thermo-siphon effect as the air becomes heated by the canister **101**. A typical airflow annulus may be in the range of about and including 2-8 inches in radial width as a non-limiting example depending on the estimated heat load of the fuel canister **100** and ventilation cooling air flow needed. The air flowrate is selected to maintain the desired canister maximum temperature limit. It bears noting that the canister support rib plates **143** maintain the annulus **122** even during occurrence of a seismic event to ensure cooling air can continue to reach the canister.

The ventilation annulus **122** extends vertically for at least the full height of the canister and preferably slightly above. The upper portion of canister **101** is laterally/radially supported and centered by a plurality of upper guide members **117** discussed below. Accordingly the canister **101** has a height approaching the full height of the cask cavity **121**, and at least greater than $\frac{3}{4}$ the height of the cavity. Annulus **122** further extends all the way down to the top plate **141** of the canister support structure **140** and is in fluid communication with the air inlet **200** of the cask in structure **140**, as further described herein.

The radially and vertically extending guide members **117** are disposed in the upper portion of the cask cavity **121**. The array of upper guide members **117** are circumferentially spaced apart and rigidly attached to the interior/internal surface **112a** of the inner shell **112** such as via welding. Guide members **117** may be formed of steel plates (e.g., lugs) or tubes, and are provided around the entire inner shell at least at the upper portion in cavity **121** for full 360 degree coverage. The inward vertical sides or edges of the guide members are configured to abuttingly engage and center the canister **101**, which prevents excessive laterally/radially movement and rattling thereof if vibrated during a seismic event, transport, or when being lifted/lowered by a crane or hoist from or into the cask internal cavity **121**. Notably, the guide members **117** further act to maintain the ventilation annulus **122** between canister **100** and inner shell **112** in the upper portion of the cask cavity **121** to preserve this airflow passage for removing heat emitted by the canister. This ensures that a continuous available flow of ambient cooling can to circulate around and flow upwards along the sides of the canister for cooling.

A radiation-shielded lid **114** is detachably coupled to the top **119** of cask body **110** and closes the normally upwardly open cavity **121** of cask **100** when in place (except for the cooling/ventilation air outlet path through the lid). Air outlet **220** of the cask ventilation system is formed through the lid. The lid **114** may have a "disk and donut" configuration in one embodiment comprising an upper annular member **114a** defining a central air outlet opening **114f** and lower disk member **114b** rigidly coupled thereto. Disk member **114b** is sized to fit inside the top end of cask internal cavity **121**. Annular lid member **114a** rests on the top **119** of the cask body **110** on sidewall **110a** when the lid is in place. More specifically, lid member **114a** is seated on annular top closure plate **119a** which is fixedly welded to the top ends of inner and outer shells **112**, **111**. Multiple fill holes **145** may be formed in closure plate **119a** for pouring the concrete liner **113** between the inner and outer shells **112**, **111** of radiation shielded cask body **110**. Lid member **114a** is detachably coupled to cask body **110** via a plurality of threaded fasteners **146** each secured to a vertical steel lifting

plate **146** embedded in the concrete liner **113** at the top of the bask body and welded to the inner and outer shells **112**, **111** (see, e.g., FIGS. **12** and **14**).

Lid **114** comprised of the annular and disk members **114a**, **114b** is a composite structure comprising a hollow metal outer housing **114c** defining an interior space filled with a radiation shielding material **114d** such as a high-density concrete liner encased by the outer housing. Other shielding materials may be used in addition to or instead of concrete. Lid **114** provides radiation shielding in the vertical upward direction, whereas the concrete liner **113** disposed between the inner and outer shells **112**, **111** provides radiation shielding in the lateral or radial direction. With exception of the concrete liner, the housing **114c** is preferably formed of a metal such as without limitation steel (e.g. carbon or stainless) capable of withstanding projectile impacts or other sources of potential damage.

According to one aspect of the nuclear waste fuel storage system, the vertical ventilated nuclear fuel storage cask **100** includes a natural circulation cooling air ventilation system (i.e. unpowered by fans/blowers) for removing decay heat emitted from the canister **101** which holds the SNF or other high level nuclear waste material. The cooling airflow provided by ambient air surrounding the cask is driven by a natural convective thermo-siphon effect in which air within the ventilation annulus **122** is heated by the canister **101** (containing the decaying SNF or other nuclear waste material) causing an upflow which draws ambient cooling air into the cask at bottom through the air inlet **200** in the canister support structure **140**.

The cask cooling air ventilation system will now further be described in further detail.

Referring generally to FIGS. **1-23** as applicable, the cask ventilation provisions include a cooling air inlet **200** formed in the bottom of cask **200** through canister support structure **140** and cooling air outlet **220** formed through the lid. Air inlet and outlet **200**, **220** are in fluid communication with ambient atmosphere and the internal cavity **121** of cask **100**, and more particularly ventilation annulus **122** formed when the nuclear waste canister **101** is in position in the cavity.

The air inlet **200** comprises downwardly open air inlet openings **201** formed through horizontal flat baseplate **115** of the canister support structure **140** which is affixed to the bottom of the cask body **110**. Air inlet openings **201** provide the fluid connection of the lower portion of cask internal cavity **121** to ambient atmosphere via the air inlet in the canister support structure. Air inlet openings **201** may be arranged in a circular array in one embodiment which is concentrically and coaxially aligned with the vertical centerline axis CL of the cask.

Air inlet **200** comprises inlet ductwork **208** collectively defined by a plurality of compound shaped air inlet ducts **202** formed within and extending through be canister support structure **140** including concrete liner **142**. The air inlet ductwork of the ventilated cask **100** therefore does not penetrate the sidewall of the cask (i.e. inner shell **112**, outer shell **111**, and concrete liner **113**) to prevent radiation streaming in the radial/lateral direction to the ambient environment where workers may be present. In the non-limiting illustrated embodiment, eight inlet ducts **202** are provided (two located within each quadrant of the cask and its internal cavity **121** (see, e.g., FIG. **13**). Other numbers of inlet ducts however may be provided in other embodiments and does not limit the invention. The inlet ducts **202** are preferably arranged in a tightly spaced circular or annular array or grouping such that the lateral spacing between adjacent ducts is less than the lateral width of each duct. This tight

grouping beneficially ensures that the cylindrical shell **103** of canister **101** is evenly and adequately cooled by a circumferentially-extending curtain of ambient cooling air, as further described herein.

The individual inlet ducts **202** of the inlet ductwork **208** in canister support structure **140** each have a compound configuration designed such that no straight line of sight exists between the internal cavity **121** of cask **100** (including ventilation annulus **122**) and the air inlet openings **201** in the baseplate **115** or ambient environment. This prevents straight line radiation streaming in the downwards direction through the air inlet ducts.

Accordingly, in one embodiment, each air inlet duct **202** may include a hollow metal body having generally Z-shaped transverse cross-sectional shape formed by, in operable fluid communication: a vertical lower entrance portion **203** fluidly coupled to a respective air inlet opening **201** in baseplate **115**; a vertical upper exit portion **204** fluidly coupled to the ventilation annulus **122** in the internal cavity **121** of the cask body **110**; and a radial/horizontal intermediate portion **205** fluidly coupled between the entrance and exit portions. Lower entrance portion **203** of each inlet duct **202** is located radially inwardly from its respective upper exit portion **204** and therefore is closer to the vertical centerline axis CL of the cask body. Inlet ducts **202** extend through the concrete liner **142** of the canister support structure **140** in the zig-zag shape shown and may be formed of steel or another suitable metal. The ducts **202** may be welded to the baseplate **115** and top plate **141** of the canister support structure before concrete is filled therebetween embedding the ducts in the concrete.

The upper exit portions **204** of air inlet ducts **202** each define an upwardly discharging air exit opening **206** which discharges and introduces ambient cooling air passing through the ducts into the bottom of internal cavity **121** of cask **100**, and more particularly the bottom of the ventilation annulus **122**. The upper exit portions **204** and exit openings **206** are therefore located adjacent to sidewall **110a** of the cask body **110** and at the bottom of the ventilation annulus. In one embodiment, ducts **202** are arranged as previously described herein such that their corresponding air exit openings **206** of the ducts concomitantly form a circular or annular array openings adjacent to cask inner shell **112** which in turn is concentrically aligned with the vertical centerline axis CL of the cask (see, e.g., FIGS. **4** and **13**). Advantageously, ambient cooling air is discharged and introduced axially and vertically upwards into the ventilation annulus (parallel to centerline axis CL) to form a circumferentially-extending cooling air curtain surrounding the canister for 360 degrees. Each quadrant of the canister is therefore equally cooled in a balanced manner to minimize or prevent localized "hot spots" on the canister shell. It bears noting that the very small gaps between adjacent air inlet ducts **202** as shown in the figures have no practical effect on effectiveness of cooling the canister since the incoming ambient cooling air between the ducts mixes upon entry into the bottom of ventilation annulus **122**.

It is further notable that introducing the ambient cooling air in the vertically and axially upwards direction into the ventilation annulus **122** of cask **100** (parallel to cask centerline axis CL) as opposed to introducing the air radially into the annulus through the sidewall of the cask **100** provides additional benefits. The present cooling air vertical introduction path in which air flows upwards parallel to the sides of the canister (and cask vertical centerline axis CL) enhances canister cooling since it creates less turbulence when compared to radial introduction of cooling air into the

11

cask which strikes the canister perpendicularly and disperses. This translates into reduced airflow resistance and a greater naturally driven convective cooling air flow rate (CFM-cubic feet per minute) via the thermo-siphon effect to cool the canister **101** and fuel assemblies therein. This is notable particularly since the passive cooling air flow is unassisted by a fan or blower. Furthermore, the vertically upwards introduction of ambient cooling air into the cask internal cavity **121** flows in the same direction as the air heated by the canister which naturally rises and flows upwards via the natural thereto-siphon effect.

According to another aspect of the cask ventilation cooling system, cask **100** is raised or elevated above the concrete base pad **130** by a plurality of standoff members **150** protruding downwards from baseplate **115** to engage the pad. Standoff members **150** collectively support the entire weight of the cask **100** and canister **101** with fuel assemblies loaded therein. In one embodiment, standoff members **150** may comprise steel plates of an elongated rectangular form as shown. However, other shaped standoff members may be used. To evenly distribute the weight of the loaded cask **100**, the standoff members **150** may comprise a circular outer array of outer standoff members **150a** and a circular inner array of inner standoff members **150b**. Standoff members **150a**, **150b** are circumferentially spaced apart with respect to the other standoff members in each of their respective arrays. Outer standoff members **150a** are spaced radially outwards from the inner standoff members **150b** on the bottom baseplate **115**. The circumferential spacing allows ambient cooling air to be drawn radially inwards beneath the baseplate **115** of the cask and upwards into the circular array of air inlet openings **201** formed therein. In one embodiment, the inner standoff members **150b** may be located closer to centerline axis CL of cask **100** than and inside of the air inlet openings **201**.

With respect to the natural thermo-siphon cooling air ventilation system, standoff members **150** form an air inlet plenum **151** beneath the cask **100** due to vertical spacing or gap between baseplate **115** and the concrete base pad **130**. The standoff members **150** are spaced apart as noted above which plays the important function of allowing ambient air to enter the plenum and reach the air inlet openings **201** of the air inlet ducts **202**. An inflow of ambient air enters the plenum **151** from a full 360 degrees around the entire bottom perimeter of the cask **100**. Cooling air is drawn through/between standoff members **150** into the plenum and then enters internal cavity **121** of the cask via the air inlet openings **201** of the ducts **202** formed in the baseplate **115**.

Advantageously, because the inlet openings **201** are formed as cuts or openings in the flat horizontal baseplate **115** of canister support structure **140**, the inlets are relatively insensitive to the direction of the wind since the ambient air first collects in the air inlet plenum **151** formed beneath the baseplate **115** before vertically rising and entering the air inlet openings. This contrasts to designs in which ventilation air inlet openings or penetrations are formed in the lateral sides of the cask body. The wind can cause air pressure to be greater on the windward side of the cask than the leeward side, thereby resulting in unbalanced and preferential flow rates of cooling air entering the cask. This can unevenly cool portions of the canister **101**, particularly if the hot spots on the SNF canister are on the leeward side of the cask which receives less cooling air. By contrast in the present vertical air inlet design of cask **100**, however, the inlet plenum **151** from which the cooling air is drawn into the cask is naturally

12

pressure balanced and the air thoroughly mixed resulting in more uniform inlet air pressure and even cooling of all sides of the canister.

Turning now to the upper end of the cask **100**, the cooling air outlet **220** of the ventilation system in lid **114** is formed by a plurality of outlet ducts **221** extending between upper annular member **114a** defining the central air outlet opening **114f** and lower disk member **114b** previously described herein. Outlet ducts **221** are in fluid communication with cask internal cavity **121** at bottom and air outlet opening **114f** at top which is in fluid communication with ambient atmosphere via a hollow tubular top weather protection cap structure **225** which forms an upwardly protruding lid extension as shown. Cap structure **225** may comprise a vertical cylindrical sidewall **226** fitted with a perforated vent screen **227** on its upper portion and preferably solid top cover plate **228** to prevent the direct ingress of rain into the cap. Vent screen **227** may have an open area of approximately 50% in one non-limiting embodiment; however, other open areas may be used. An open interior **229** is defined inside cap structure **225** which is in fluid communication at bottom with the air outlet opening **114f** in the lid upper annular member **114a** and laterally/radially to ambient atmosphere through the vent screen **227**.

Outlet ducts **221** in lid **114** have a circuitous shape in transverse cross section such that no straight line of sight exists between cask internal cavity **121** and outlet opening **114f** or the ambient environment. This prevents straight line radiation streaming in the upward direction as exemplified by the flow path followed by the heated cooling air described below.

A method for operation of the natural convective thermo-siphon air ventilation system will now be summarized. FIG. **19** is a cross sectional view of cask **100** showing the cooling air flow path therethrough and corresponding directional flow arrows.

In operation, referring to FIG. **19** and other applicable figures, ambient cooling air is first drawn radially inwards into inlet plenum **151** between standoff members **150** from the ambient environment a full 360 degrees around the bottom of the cask **100**. The air then mixes first and flows vertically upwards through air inlet openings **201** in baseplate **115** of canister support structure **140** and enters the inlet ducts **202**. The air flows vertically upwards, then radially outwards, and finally vertically upwards in ducts **202**. The still cool ambient air is drawn into the bottom of ventilation annulus **122** of cask **100** from the annular array of upward discharging duct exit openings **206** of the inlet ducts.

Canister **101** heats the incoming air in ventilation annulus **122** which rises upwards and collects in an annular air outlet plenum **222** formed within cask internal cavity **121** between inner shell **112** and lower disk member **114b** of the lid. The now heated cooling air flows vertically upwards in the plenum and then turns radially inwards through outlet duct **221** to central outlet opening **114f** in upper annular member **114a** of the lid. The heated cooling air continues to flow vertically upwards inside cap structure **225** and then is discharged radially/laterally outwards through vent screens **227** to ambient atmosphere. Heating of the air in the ventilation annulus **122** by the fuel assemblies within the canister **101** drives the foregoing air circulation continuously as long as heat is emitted by the canister.

According to another aspect of the nuclear waste storage system, the air inlet region of cask **100** may be supplemented where needed for increased radiation blockage with photon attenuators. These may be perimetrically positioned in

13

spaces beneath the cask body **110** and only in locations of potential increased radiation levels such as along cask storage area borders or fences in close proximity to the loaded casks containing SNF or other high level radioactive waste. FIG. **17** shows the underside of a certain embodiment of cask **100** including arcuately curved radiation photon scattering attenuators **160**. The attenuators provided are each fixedly coupled between a pair of the radial plate outer standoff members **150a** in the outer array of standoffs on the bottom baseplate **115** previously described herein. A pair of attenuators is shown in this figure; however, more or less can be used as needed. The attenuators **160** are configured with open areas to allow the ambient cooling air to flow inwards into the bottom air inlet plenum **151** of the natural ventilation system towards the air inlet **200** in canister support structure **140**. In the non-limiting illustrated embodiment, each attenuator **160** may comprise an arcuately curved outer support bar **161** and optional inner support bar **163** which may each be welded at their ends to opposing standoff members **150a** welded in turn to the bottom of baseplate **115**. A plurality of vertically orientated flat deflector plates **162** are welded to and arcuately spaced apart on the bars **161**, **163** as shown. Plates **162** may be optionally welded to baseplate **115** in additional if needed for added stability and support. In some embodiments, the bottom surfaces of the outer support bars **161** may be flush with the bottom surfaces of the outer standoff members **150a** as shown so that the bars rest on the concrete base pad **130** with the standoffs. This provides added support for the attenuators **160** and cask. In one embodiment, support bars **161**, **163** and deflector plates **162** may be formed of metal such as steel or another suitable metal. As shown in FIG. **17**, attenuators **160** are only located where required and not necessarily around the entire perimeter of the cask bottom.

FIG. **18** shows gridded radiation photon scattering duct attenuator **170** installed in the air outlet **220** of the cask ventilation system. The duct attenuator **170** is formed by an orthogonally intersecting array of steel or other metallic flat duct deflector plates **171** which may be fitted inside central air outlet opening **114f** in lid **114**. FIGS. **22-23** show a similar gridded duct attenuator **170** installed in inlet ducts **202** of canister support structure **140** at both the air outlet **206** and air inlet **201** of each duct.

Features and advantages of the present cask with ambient cooling air ventilation system include but are not limited to the following. The high-density concrete liners **113** and **142** of the cask sidewall and canister support structure **140** respectively may comprise hematite (iron oxide compound Fe_2O_3) and/or other iron-containing aggregates which substantially boost the thermal conductivity of the liners resulting in a significant rate of conduction heat transfer from the inside surface of the cask to the outside surface. The heat duty of the cask is therefore accordingly increased to dissipate heat emitted by the canister **101**. Cask **100** has superior radiation shielding performance attributable to no lateral/radial or vertical streaming paths for radiation emanating from the nuclear fuel stored in the canister inside the cask. This also creates the absence of any open intrusion path for small penetrant missiles that can reach the nuclear fuel inside the cask. Air inlet and outlet openings optionally equipped with duct photon attenuators **170** which act to further attenuate radiation thereby decreasing ambient levels of radiation. Any minute dose allowed from the bottom region of the cask may be further reduced by using arcuately curved photon attenuators **170** at the periphery of the air inlet plenum **151** beneath the cask. The penetration for the air outlet in the top lid features the "disk & donut" geometry

14

previously described herein with a large overlap in the planar horizontal direction at the cask body **110** to lid **114** interface such that there is no path for direct vertically upwards streaming of radiation from the cask internal cavity holding the canister to the ambient environment. The structurally robust concrete and steel disk part of the lid also serves to block any incoming missile or projectile. The width of the air inlet and outlet flow passages (e.g. ducts) can be optimized to meet the needed heat duty of cask **100** without permitting excessive amounts of diffused radiation inside the cask from reaching the ambient environment. The ventilated cask **100** is configured and suited for sheltered or unsheltered deployment on the concrete storage or base pad **130**. The cask can therefore be stored inside a building that has adequate ventilation, or in unsheltered storage facilities out in open air to facilitate improved ventilation and cooling of the cask.

While the foregoing description and drawings represent some example systems, it will be understood that various additions, modifications and substitutions may be made therein without departing from the spirit and scope and range of equivalents of the accompanying claims. In particular, it will be clear to those skilled in the art that the present invention may be embodied in other forms, structures, arrangements, proportions, sizes, and with other elements, materials, and components, without departing from the spirit or essential characteristics thereof. In addition, numerous variations in the methods/processes described herein may be made. One skilled in the art will further appreciate that the invention may be used with many modifications of structure, arrangement, proportions, sizes, materials, and components and otherwise, used in the practice of the invention, which are particularly adapted to specific environments and operative requirements without departing from the principles of the present invention. The presently disclosed embodiments are therefore to be considered in all respects as illustrative and not restrictive, the scope of the invention being defined by the appended claims and equivalents thereof, and not limited to the foregoing description or embodiments. Rather, the appended claims should be construed broadly, to include other variants and embodiments of the invention, which may be made by those skilled in the art without departing from the scope and range of equivalents of the invention.

What is claimed is:

1. A method for operating a passively ventilated nuclear fuel storage system comprising:
 - providing a cask comprising an internal cavity and an ambient air ventilation system in fluid communication with the internal cavity and atmosphere;
 - inserting a canister containing nuclear waste emitting heat into the internal cavity of a cask and onto a canister support structure fixedly coupled to the cask;
 - drawing ambient cooling air into an air inlet plenum formed beneath the cask;
 - flowing the cooling air upwards from the air inlet plenum through the canister support structure into the internal cavity of the cask;
 - heating the cooling air in the internal cavity of the cask; and
 - discharging the heated cooling air to atmosphere through a lid coupled to a top of the cask.
2. The method according to claim 1, wherein the cooling air is heated by the canister in a ventilation annulus formed between the cask and canister in the internal cavity.

3. The method according to claim 1, wherein the cooling air flows vertically upwards into the ventilation annulus from the canister support structure.

4. The method according to claim 1, wherein the cooling air flows into the internal cavity of the cask through plurality of air inlet ducts formed vertically through the canister support structure, and the cooling air flows outwards from the internal cavity through a plurality of air outlet ducts in the lid. 5

5. The method according to claim 4, wherein the air inlet ducts and air outlet ducts are each arranged in a circumferentially-extending annular array in the canister support structure and lid, respectively. 10

6. The method according to claim 5, wherein no straight line of sight exists through the air inlet and outlet ducts to prevent radiation streaming. 15

7. The method according to claim 1, wherein the drawing step comprises drawing air radially inwards into the air inlet plenum which is formed between a baseplate of the canister support structure and concrete base pad which supports the canister. 20

8. The method according to claim 7, wherein the air inlet plenum is formed by a plurality of standoff members which elevate the baseplate apart from the base pad.

9. The method according to claim 1, wherein there are no penetrations in a sidewall of the cask associated with the ventilation system. 25

* * * * *